

Pg 126

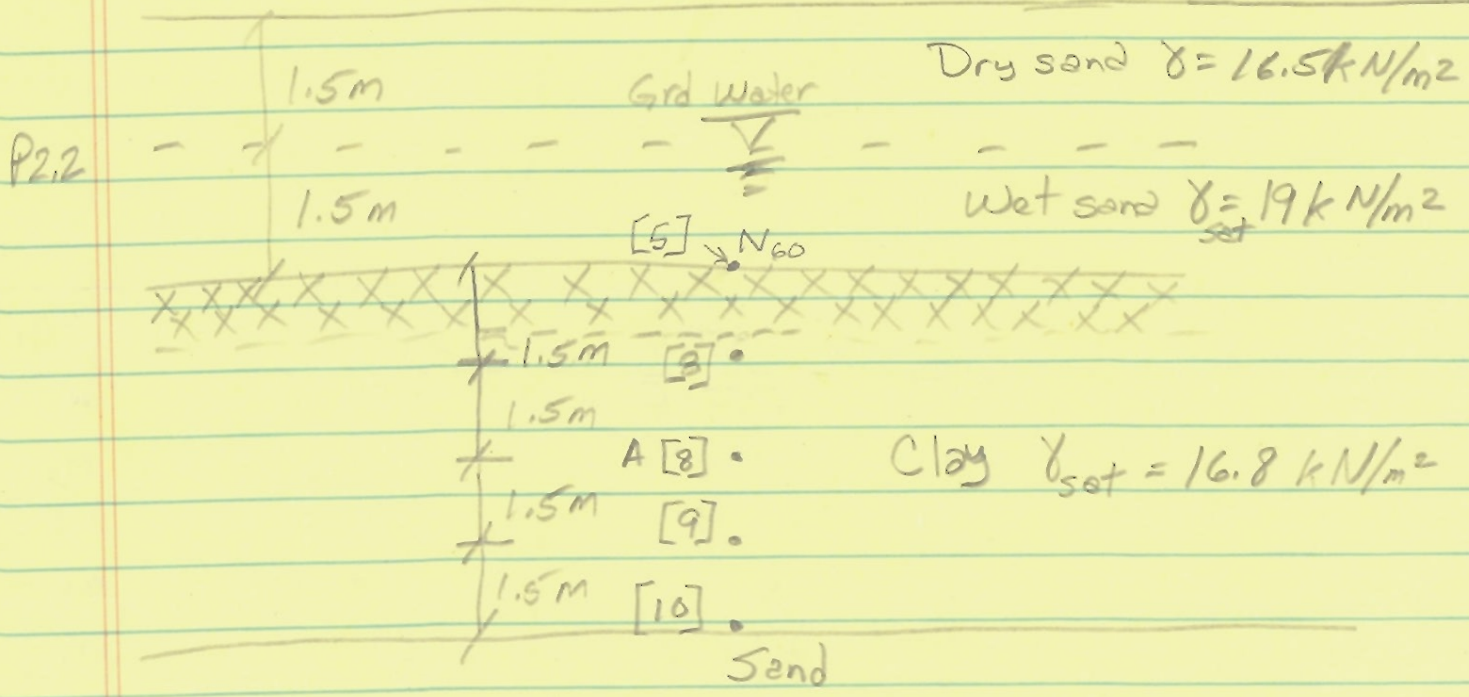
#2.2

A soil profile is shown Fig P2.2 with standard penetration numbers in a clay layer. Use Eq 2.8 & 2.9 to determine the variation of c_u & OCR with depth. What is average c_u & OCR?

define c_u = undrained cohesion (undrained shear strength)
 OCR = over consolidation ratio $\left(\frac{\text{Preconsolidation pressure, } \sigma'_p}{\text{effective over burden pressure, } \sigma'_o} \right)$

[2.8] $\frac{c_u}{P_a} = 0.29 N_{60}^{0.72}$ $P_a = \text{atmospheric pressure} \approx 100 \text{ kN/m}^2 \approx 2,000 \text{ #/in}^2$
 $\therefore c_u = 0.29 \cdot P_a \cdot N_{60}^{0.72}$

[2.9] $OCR = 0.193 \left(\frac{N_{60}}{\sigma'_o} \right)^{0.689}$ $\sigma'_o = \text{effective vertical stress in MN/m}^2 \text{ or kN/m}^2/1000 = h\gamma - h\gamma_{\text{water}}$



#2.2
Contin.

$$C_u = 0.29 P_0 N_{60}^{0.72}$$
$$3.0m \quad C_u = (0.29)(100 \text{ kN/m}^2)(5)^{0.72} = \boxed{92.397}$$
$$OCR = 0.193 \left(\frac{5}{(1.5m)(16.5 \text{ kN/m}^3) + (1.5)(19) - (1.5m)(9.81 \text{ kN/m}^3)/1000} \right)^{0.689}$$
$$OCR = 0.193 \left(\frac{5 \times 1000}{38.535} \right)^{0.689} = \boxed{5.514}$$

$$4.5m \quad C_u = (0.29)(100 \text{ kN/m}^2)(8)^{0.72} = \boxed{129.605}$$
$$OCR = (0.193) \left(\frac{8 \times 1000}{(1.5 \times 16.5) + (1.5 \times 19) + (1.5 \times 16.8) - (3.0)(9.81)} \right)^{0.689}$$
$$= 0.193 \left(\frac{8000}{49.02} \right)^{0.689} = \boxed{6.458}$$

$$6.0m \quad C_u = 0.29(100 \text{ kN/m}^2)(8)^{0.72} = \boxed{129.605}$$
$$OCR = 0.193 \left(\frac{8 \times 1000}{(1.5 \times 16.5) + (1.5 \times 19) + (3 \times 16.8) - (4.5 \times 9.81)} \right)^{0.689}$$
$$= 0.193 \left(\frac{8000}{59.5} \right)^{0.689} = \boxed{5.651}$$

$$7.5m \quad C_u = 0.29(100 \text{ kN/m}^2)(9)^{0.72} = \boxed{141.076}$$
$$OCR = 0.193 \left(\frac{9 \times 1000}{(1.5 \times 16.5) + (1.5 \times 19) + (4.5 \times 16.8) - (6.0 \times 9.81)} \right)^{0.689}$$
$$= 0.193 \left(\frac{9000}{69.99} \right)^{0.689} = \boxed{5.480}$$

$$9m \quad C_u = 0.29(100 \text{ kN/m}^2)(10)^{0.72} = \boxed{152.194}$$
$$OCR = 0.193 \left(\frac{10 \times 1000}{(1.5 \times 16.5) + (1.5 \times 19) + (6 \times 16.8) - (7.5 \times 9.81)} \right)^{0.689}$$
$$= 0.193 \left(\frac{10,000}{80.475} \right)^{0.689} = \boxed{5.353}$$

C_u (KN/m²) | OCR (m³/mN)

3.0m 92.397 5.514

4.5m 129.605 6.458

6.0m 129.605 5.651

7.5m 141.076 5.480

9.0m 152.194 5.353

→ [AVG 128.995 5.691]

#2.6

The given table is the variation of the field standard penetration number (N_{60}) in a Sand deposit

Depth	δ (kN/m ³)	σ'_o kN/m ² /1000	P_a kN/m ²	N_{60}	C_N	D_r %
1.5	18	27	100	6	1.575	50.55
3.0	18	54	100	8	1.30	51.67
4.5	18	81	100	9	1.105	49.20
6.0	18	108	100	8	0.962	43.17
7.9	20.2	127.741	100	13	0.878	52.23
9.0	20.2	139.17	100	14	0.836	52.70

$$[2.12] \quad C_N = \frac{2}{1 + \left(\frac{\sigma'_o}{P_a}\right)}$$

Depth	σ'_o
1.5	$1.5 \times 18 = 27$
3.0	$3.0 \times 18 = 54$
4.5	$4.5 \times 18 =$
6.0	$6.0 \times 18 =$
7.9	$(6 \times 18) + (1.9 \times 20.2) - (1.9 \times 9.81)$
9.0	$(6 \times 18) + (3.0 \times 20.2) - (3.0 \times 9.81)$

$$[2.20] \quad D_r = \left\{ \frac{N_{60}}{\left[17 + 24 \left(\frac{\sigma'_o}{P_a} \right) \right]} \right\}^{0.5}$$

$$1.5m \quad C_N = \frac{2}{1 + \left(\frac{27}{100}\right)} = 1.575$$

$$D_r = \left\{ \frac{6}{\left[17 + 24 \left(\frac{27}{100} \right) \right]} \right\}^{0.5} \times 100 = 50.55\%$$

$$3.0m \quad C_N = \frac{2}{1 + \left(\frac{54}{100}\right)} = 1.2987$$

$$D_r = \left\{ \frac{8}{\left[17 + 24 \left(\frac{54}{100} \right) \right]} \right\}^{0.5} \times 100 = 51.674$$

$$4.5m \quad C_N = \frac{2}{1 + \left(\frac{81}{100}\right)} = 1.105$$

$$D_r = \left\{ \frac{9}{\left[17 + 24 \left(\frac{81}{100} \right) \right]} \right\}^{0.5} \times 100 = 49.697$$

#2.10

The following are details for a soil deposit in sand

Depth	Effective Overburden	Field Standard N_{60}
3.0m	55	9
4.5m	82	11
6.0m	98	12

$$C_u = 2.8 \quad \& \quad OCR = 2$$

$$[2.19] \quad D_r \% = 12.2 + 0.75 \left[222 N_{60} + 2311 - 711 \cdot OCR - 779 \left(\frac{\sigma'_0}{P_a} \right) - 50 C_u^2 \right]^{0.5}$$

$$3.0m \quad D_r \% = 12.2 + 0.75 \left[222(9) + 2311 - 711(2) - 779 \left(\frac{55}{100} \right) - 50(2.8)^2 \right]^{0.5}$$

$$= 46.294 \%$$

$$4.5m \quad D_r \% = 12.2 + 0.75 \left[222(11) + 2311 - 711(2) - 779 \left(\frac{82}{100} \right) - 50(2.8)^2 \right]^{0.5}$$

$$= 48.170 \%$$

$$6.0m \quad D_r \% = 12.2 + 0.75 \left[222(12) + 2311 - 711(2) - 779 \left(\frac{98}{100} \right) - 50(2.8)^2 \right]^{0.5}$$

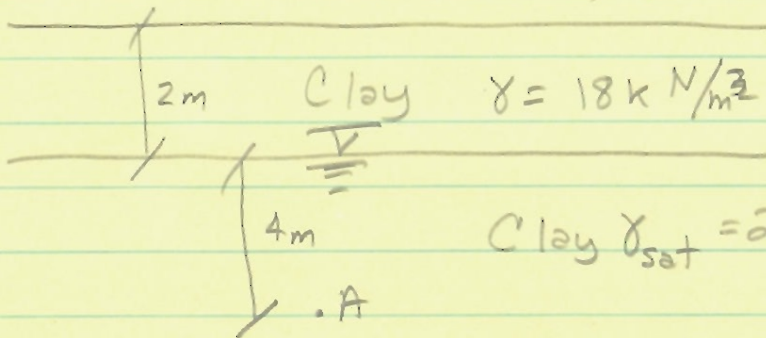
$$= 48.924 \%$$

#2.12

The soil profile below, if the cone penetration resistance (q_c) @ A = 0.8 MN/m^2 (electric cone)

A. Estimate cohesion, C_u

B. Overconsolidation ratio, OCR



$N_k = 15$ (electric cone)

$$\sigma_0 = (2 \times 18) + (4 \times 20) = 116 \text{ kN/m}^2$$

$$A. [2.51] C_u = \frac{q_c - \sigma_0}{N_k} = \frac{0.8 \times 1000 - 116}{15} = \boxed{45.6 \text{ kN/m}^2}$$

$$B. [2.55] \text{OCR} = 0.37 \left(\frac{q_c - \sigma_0}{\sigma'_0} \right)^{1.01}$$

$$= 0.37 \left(\frac{(0.8 \times 1000) - 116}{116 \text{ kN/m}^2 - (4 \times 9.81)} \right)^{1.01}$$

$$\text{OCR} = 0.37 \left(\frac{684}{76.76} \right)^{1.01} = \boxed{3.370}$$