



Standard Guide for Depth Profiling in Auger Electron Spectroscopy¹

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1. Scope

1.1 This guide covers procedures used for depth profiling in Auger electron spectroscopy.

1.2 Guidelines are given for depth profiling by the following:

	Section
Ion Sputtering	6
Angle Lapping and Cross-Sectioning	7
Mechanical Cratering	8
Nondestructive Depth Profiling	9

1.3 *This standard does not purport to address all of the safety problems, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Referenced Documents

2.1 ASTM Standards:

- E 673 Terminology Relating to Surface Analysis²
- E 684 Practice for Approximate Determination of Current Density of Large-Diameter Ion Beams for Sputter Depth Profiling of Solid Surfaces²
- E 827 Practice for Elemental Identification by Auger Electron Spectroscopy²
- E 1634 Guide for Performing Sputter Crater Depth Measurements²

3. Terminology

3.1 Definitions:

3.1.1 For definitions of terms used in this guide, refer to Terminology E 673.

4. Summary of Guide

4.1 In ion sputtering, the surface layers are removed by ion bombardment in conjunction with Auger analysis.

4.2 In angle lapping, the surface is lapped or polished at a small angle to improve the depth resolution as compared to a cross section.

4.3 In mechanical cratering, a spherical or cylindrical crater is created in the surface using a rotating ball or wheel. The sloping sides of the crater are used to improve the depth resolution as in angle lapping.

4.4 In nondestructive techniques, different methods of varying the electron information depth are involved.

5. Significance and Use

5.1 Auger electron spectroscopy yields information concerning the chemical and physical state of a solid surface in the near surface region. Nondestructive depth profiling is limited to this near surface region. Techniques for measuring the crater depths and film thicknesses are given in (35).

5.2 Ion sputtering is primarily used for depths of less than the order of 1 μm .

5.3 Angle lapping or mechanical cratering is primarily used for depths greater than the order of 1 μm .

5.4 The choice of depth profiling methods for investigating an interface depends on surface roughness, interface roughness, and film thickness (1).³

6. Ion Sputtering

6.1 First introduce the specimen into a vacuum chamber equipped with an Auger analyzer and an ion sputtering gun. Align the ion beam using a sputtering target or a Faraday cup, paying careful attention to the relative spot size of the electron beam, ion beam, and Faraday cup and their respective orientations to ensure accurate convergence of the two beams at the specimen surface.

6.1.1 Place the specimen in front of the Auger analyzer and direct the ion gun towards the analysis area. If the ion beam is not normal to the specimen surface then possible shadowing of the analysis area from the ion beam must be considered.

6.2 Choose the elements to be investigated from previous experience or from an initial Auger electron spectrum or an energy-dispersive X-ray spectrum since the latter spectrum can reveal additional elements present at depths greater than those that contribute to the Auger electron spectrum (2). Select a specific transition for each element. During the depth profiling, record the peak-to-peak heights for Auger derivative data, or peak heights or peak areas for $N(E)$ data. The data may be

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² Annual Book of ASTM Standards, Vol 03.06.

³ The boldface numbers in parentheses refer to the list of references at the end of this guide.

gathered during continuous sputtering or between timed sputter segments. Results may vary between the two techniques.

6.2.1 One source of their difference is due to the presence of ion-induced electrons during continuous sputter depth profiling, especially at low-electron kinetic energies, that can become comparable in intensity to the electrons induced by the probing incident electron beam. Unless one or the other of the excitation beams is modulated and detected synchronously these two types of emitted electrons are difficult to distinguish. These ion-induced electrons usually form a featureless background that rises steeply as their kinetic energy decreases, but sometimes ion-induced Auger peaks might be present whose lineshape may be different from those produced by the electron beam (3). As a result, care must be taken during continuous sputtering to ensure reliable results. Another source of difference is due to the buildup of adsorbed species during the data acquisition time in the discontinuous sputter depth profile mode (4). If portions of the ion-eroded surface expose very reactive phases, then Auger peaks due to adsorbed species, for example, oxygen or carbon, or both, will appear in the spectra and mask the actual depth distribution.

6.2.2 It is advisable when analyzing an unknown specimen to periodically examine survey scans to detect any new elements that were not present in the initial survey scan and to determine if any of the Auger peaks have been displaced outside of their analysis windows (5).

6.3 Crater-edge profiling of the sputter-formed crater by using Auger line scans is a technique similar to the analysis of the mechanically formed craters in Section 8 (6). Forming the crater by sputtering may introduce the additional complications of ion-induced damage and asymmetric crater dimensions.

6.4 If specimen rotation is used to reduce ion-induced roughness, then the rotational speed, rotation axis runout relative to ion beam sputtered area or wobble and data acquisition rate should be reported (7 and 8).

6.5 Identify the elements in the survey scans using Practice E 827.

6.6 The Auger data and the sputtering conditions should be reported as described in Practice E 996.

6.7 There is extensive information available in the literature on the effects of ion bombardment on solid surfaces (9-14).

6.8 Special care must be exercised whenever specimen temperature changes are present because effects due to surface diffusion, surface segregation or diffusion limited bulk processes such as point defect migration can occur and dramatically alter the specimen composition, even over depths larger than the ion beam penetration depth which is typically a few nanometers (15 and 16). The concept of preferential sputtering in multielement, single-phase specimens has altered significantly so that chemical effects such as surface segregation are considered to be at least as important as physical effects such as mass differences in the evolution of the near surface composition during sputter depth profiling (17-20). Since the probing depths in Auger electron spectroscopy are usually smaller than the ion-penetration depth these effects are very important in any interpretation of Auger signal intensity in terms of composition during ion-beam profiling. Computer

modelling of these and other ion-induced phenomena has been extensively studied and has provided new insights into this field (21 and 22).

6.8.1 It should be determined for each specimen if compositional changes or other sputter effects are likely to occur. It may be possible to minimize these effects in some instances by adjusting the sputtering parameters.

6.9 Ion guns used in Auger analysis are normally self-contained units capable of producing a focused beam of ions. The specimen is not used as an anode for the gun. Many ion guns are able to raster the ion beam. A rastered ion beam will produce a more uniform ion current distribution on the specimen surface in the region of analysis.

6.10 If the ion gun is differentially pumped, the vacuum pumps may be left on during sputtering, removing most of the sputtered gases. If not, then the chamber must be back filled with gas and provisions for removing the sputtered active gases must be considered. Titanium sublimation is effective in removing these gases.

6.11 Noble gas ions are normally used in sputtering and the most commonly used gas is argon. Xenon is occasionally used with high beam energies when rapid sputtering is needed. Active gases such as oxygen and metal ions are used in special circumstances.

6.11.1 Ion energies commonly used for depth profiling using noble gases are in the range from 1 to 5 keV where lower ion energies are usually preferred for improved depth resolution. Higher ion energies usually can be obtained with higher ion currents and less preferential sputtering.

6.11.2 Ion beam current density can be measured by a Faraday cup or by following Practice E 684.

6.11.3 The sputter rate is needed to calibrate the depth scale (33, 34, Guide E 1634) when depth profiling using ion sputtering. Several reference standards are available for this purpose. One reference material consists of 30 and 100-nm thick tantalum pentoxide films (23).⁴ Another reference material is an alternating nickel and chromium thin film structure; each layer is nominally 50-nm thick.⁵

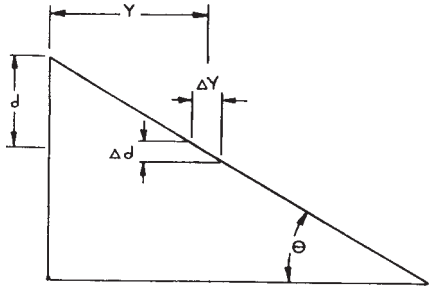
7. Angle Lapping and Cross-Sectioning

7.1 In cross-sectioning, polish the specimen perpendicular to the interface, while in angle lapping, polish the specimen at an angle to increase the depth resolution as shown in Fig. 1 (24). Polishing usually includes the use of silicon carbide papers, diamond paste, and alumina. Use progressively finer polishing particles to obtain the desired surface finish. Possible limitations of the techniques include smearing of material across the interface, surface roughness, and the electron probe diameter limiting the spatial resolution.

7.2 In angle lapping mount the specimen on a flat gage block and measure the angle with a collimator. The accuracy depends on the flatness of the specimen. In practice an angle of 0.1° can be accurately measured.

⁴ Available from the National Physical Laboratory, Teddington, Middlesex, England. Listed as Certified Reference Material NPL No. S7B83, BCR No. 261.

⁵ Available from the National Institute of Standards and Technology, U.S. Department of Commerce, Gaithersburg, MD 20899. Listed as NIST Standard Reference Material 2135.



NOTE 1—In practice, the angle θ is much smaller than shown, being of the order of 1°

FIG. 1 Cross Section of Angle-Lapped Specimen

7.3 The depth, d , is given by the following equation:

$$d = Y \tan \theta \quad (1)$$

where (in Fig. 1) θ is the lapped angle and Y is the distance from the edge.

7.4 The depth resolution, Δd , is given by the following equation:

$$\Delta d = \Delta Y \tan \theta \quad (2)$$

where ΔY includes the electron beam diameter and uncertainties in position that may be due to errors in specimen or electron beam positioning.

7.5 Auger analysis can include line scans and point analysis along the lapped surface. Perform the analysis by either moving the specimen using micrometer adjustments or by electronically moving the electron beam.

7.6 Ion sputtering (Section 6) is often used in conjunction with angle lapping to remove contaminants and to investigate interfaces beneath the lapped surfaces.

7.7 Consideration should be given if specimen mounting methods, for example, plastic embedding media, are used which may employ high vapor pressure materials. Out-gassing of the media as well as trapped gases between the media and the specimen may require complete removal of the mounting materials prior to analysis.

8. Mechanical Cratering

8.1 Ball Cratering:

8.1.1 First mount the specimen in a device where a rotating steel ball can be placed against its surface. Commercial apparatus is available that uses a rotating shaft with a notch that holds the ball and spins it. The rotational speed and the force against the specimen can be adjusted (25).

8.1.2 Coat the ball with an abrasive material to improve the cratering rate. In practice diamond paste is used with a particle size of 0.1 to 1 μm . The larger particle sizes will give the most rapid cratering rates and the finer particle sizes will give the smoothest crater wall surface. The coarser pastes can be used first to form the crater and the fine pastes can be used to smooth the crater wall. As with cross-sectioning and angle lapping, consideration should be given to the possibility of smearing material across the cratered surface.

8.1.3 The geometry of the crater is shown in Fig. 2. The depth of the crater, d , is given by the following equation:

$$d = D^2/8R \quad (3)$$

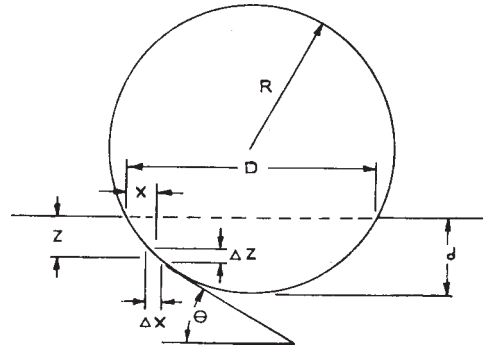


FIG. 2 Cross Section of Specimen After Ball-Cratering Using a Sphere of Radius, R , to a Depth, d

where:

D = the diameter of the crater,

R = the radius of the ball, and

$R \gg D/2$.

8.1.4 The Auger analysis is the same as described in 7.5 and 7.6.

8.1.5 The depth at any point in the analysis, Z , is given by the following equation (1):

$$Z = (R^2 - x^2 + Dx - D^2/4)^{1/2} - (R^2 - D^2/4)^{1/2} \quad (4)$$

where x is the lateral distance from the crater edge. The depth may also be given by the approximation as follows:

$$Z = x(D - x)/2R \quad (5)$$

8.1.6 The depth resolution, ΔZ , is given by the following equation:

$$\Delta Z = \Delta x \tan \theta \quad (6)$$

where Δx includes the electron beam diameter and other uncertainties in lateral position and θ is the taper angle. In contrast to angle lapping (Section 7), the taper angle, which is defined as the angle between the surface and the tangent to the crater, varies in value along the crater wall. Its value is given by the following equation:

$$\sin \theta = (0.5D - x)/2R \quad (7)$$

The best resolution is when θ is the smallest at the crater bottom.

8.2 *Radial Sectioning*—A technique similar to ball cratering that uses a cylindrical grinding tool instead of a spherical one (26).

9. Nondestructive Depth Profiling

9.1 Methods for nondestructive depth profiling with Auger electron spectroscopy are based upon varying the effective electron escape depth from the specimen and are limited to characterizing the outermost 2 to 5 nm.

9.2 For certain elements, a depth dependence may be found by examining Auger transitions of different energies (27). The lower energy Auger electrons will have a shallower escape depth than the more energetic electrons and therefore, different transitions for the same element will have different sampling depths.

9.3 The sampling depth may also be varied to a limited degree by varying the incident electron beam energy to produce a weak depth dependence in the excitation volume of the specimen (28).

9.4 Angle-resolved Auger electron spectroscopy, which involves varying the collected take-off angle of the emitted electrons, has been used for depth profiling (29), but the technique is limited due to surface roughness and an often observed angular anisotropy in the Auger signal strength (30, 31).

9.5 A general formulation that incorporates electron-solid interactions to characterize the low kinetic energy loss features

of an Auger peak can be inverted to produce a nondestructive model depth profile within a depth of almost five times the inelastic mean free path. The technique has been reported (32) to be able to distinguish island growth from layer-by-layer growth of adsorbed species.

10. Keywords

10.1 angle lapping; angle-resolved AES; Auger electron spectroscopy; ball cratering; compositional depth profiling; cross sectioning; depth profiling; depth resolution; sputter depth profiling; sputtering; thin films

REFERENCES

- (1) Lea, C., and Seah, M. P., "Optimized Depth Resolution in Ion-Sputtered and Lapped Compositional Profiles with Auger Electron Spectroscopy," *Thin Solid Films*, Vol 75, 1981, pp. 67–86.
- (2) Kirschner, J., and Itzkorn, H., "Thin Film Analysis: from 'Sputter Profiles' to 'Depth Profiles' by Combined Auger/X-ray Analysis," *Proceedings of the 7th International Vacuum Congress and 3rd International Conference on Solid Surfaces*, Vienna, 1977, pp. 2213–2216.
- (3) Aizana, T., Tsuno, T., Daimon, H., and Ino, S., "Si (111) 7×7 and Si(111) $\sqrt{3} \times \sqrt{3}$ —Al Surface—Structure Analysis by Ion-induced Auger-Electron Spectroscopy," *Physical Review B*, Vol 36, 1987, pp. 9107–9114.
- (4) Holloway, P. H., and Stein, H. J., "Quantitative Detection of Oxygen in Silicon Nitride on Silicon," *Journal of the Electrochemical Society*, Vol 123, 1976, pp. 723–728.
- (5) Lea, C., "Composition-Depth Profiling Using Auger Electron Spectroscopy," *Metal Science*, Vol 17, 1983, pp. 357–367.
- (6) Taylor, N. J., Johannessen, J. S., and Spicer, W. E., "Crater-Edge Profiling in Interface Analysis Employing Ion-Beam Etching and AES," *Applied Physics Letters*, Vol 29, No. 8, 1976, pp. 497–499.
- (7) Zalar, A., "Improved Depth Resolution by Sample Rotation During Auger Electron Spectroscopy Depth Profiling," *Thin Solid Films*, Vol 124, 1985, pp. 223–230.
- (8) Geller, J. D., and Veisfeld, N., "Depth Resolution Improvements Using Specimen Rotation During Depth Profiling," *Surface and Interface Analysis*, Vol 14, 1989, pp. 95–98.
- (9) "Sputtering by Particle Bombardment I," *Topics in Applied Physics*, Ed. R. Behrisch, Vol 47, Springer, New York, 1981.
- (10) "Sputtering by Particle Bombardment II," *Topics in Applied Physics*, Ed. R. Behrisch, Vol 52, Springer, New York, 1983.
- (11) Bevolo, A. J., "Ion/Solid Interactions in Surface Analysis," in *Characterization of Semiconductor Materials*, Vol 1, Chapter 4, Ed. G. E. McGuire, Noyes, New Jersey, 1989.
- (12) Wittmaack, K., "Beam Induced Broadening Effects in Sputter Depth Profiling," *Vacuum*, Vol 34, 1984, pp. 119–137.
- (13) "Thin Film and Depth Profile Analysis," *Topics in Current Physics*, Vol 37, Ed. O. Oeschner, Springer, New York, 1984.
- (14) Zalm, P. C., "Quantitative Sputtering," *Surface and Interface Analysis*, Vol 11, 1988, pp. 1–24.
- (15) Kirschner, J., "Surface Segregation and Its Implications for Sputtering," *Nuclear Instruments and Methods in Physics Research*, Vol B7/8, 1985, pp. 742–749.
- (16) Lam, N. Q., and Wiedersich, H., "Bombardment Induced Segregation and Redistribution," *Nuclear Instruments and Methods in Physics Research*, Vol B18, 1987, pp. 471–485.
- (17) Shimizu, R., "Preferential Sputtering," *Nuclear Instruments and Methods in Physics Research*, Vol B18, 1987, pp. 486–495.
- (18) Lam, N. Q., "Ion Bombardment Effects in the Near-Surface Composition During Sputter Profiles," *Surface and Interface Analysis*, Vol 12, 1988, pp. 65–77.
- (19) Kelly, R., "Bombardment-Induced Compositional Change with Alloys, Oxides, Oxysalts, and Halides II. The Role of Segregation," *Nuclear Instruments and Methods in Physics Research*, Vol B39, 1989, pp. 43–56.
- (20) Kelly, R., "Bombardment-Induced Compositional Change with Alloys, Oxides, Oxysalts, and Halides III. The Role of Chemical Driving Forces," *Materials Science and Engineering*, Vol 175A, 1989, pp. 11–24.
- (21) Averbeck, R. S., and Seidman, D. N., "Energetic Displacement Cascades and Their Roles in Radiation Effects," *Materials Science Forum*, Vol 15/16, 1987, pp. 963–984.
- (22) Anderson, H. H., "Computer Simulations of Atomic Collisions in Solids with Special Emphasis on Sputtering," *Nuclear Instruments and Methods in Physics Research*, Vol B18, 1987, pp. 321–343.
- (23) Hunt, C. P., Anthony, M. T., and Seah, M. P., "AES and XPS Depth Profiling Certified Reference Material," *Surface and Interface Analysis*, Vol 6, No. 2, 1984, pp. 92–93.
- (24) Levenson, L. L., "Thick Coating Analysis with Scanning Auger Spectroscopy," *Scanning Electron Microscopy*, Part 3, 1984, pp. 67–86.
- (25) Walls, J. M., Brown, I. K., and Hall, D. D., "The Application of Taper-Sectioning Techniques for Depth Profiling Using Auger Electron Spectroscopy," *Applications of Surface Science*, Vol 15, Nos. 1–4, 1983, pp. 93–107.
- (26) Whitelam, Frank E., "Using Radial Sectioning to Measure Thin Layers," *Metal Progress*, Vol 1278, 1985, pp. 45–50.
- (27) Holloway, P. H., "Thickness Determination of Ultrathin Films by Auger Electron Spectroscopy," *Journal of Vacuum Science and Technology*, Vol 12, 1975, pp. 1418–1422.
- (28) Nassiopoulou, A. G., and Cazaux, J., "Slow Electron-Energy-Loss Spectroscopy for Surface Microanalysis," *Surface Science*, Vol 149, 1985, pp. 313–325.
- (29) Berghaus, T., Neddermeyer, H., Radlik, W., and Rogge, V., "Study of Surface Composition of Iron-Based Metallic Glasses by Means of UV Photoemission, Angle-Resolved Auger Electron and Ion Scattering Spectroscopy," *Physica Scripta*, Vol 28, 1983, pp. 194–196.
- (30) Doern, F. E., Kover, L., and McIntyre, N. S., "Channeling Effects in Polycrystalline Copper—A Serious Impediment to Quantitative Auger Analysis," *Surface and Interface Analysis*, Vol 6, 1984, pp. 282–285.
- (31) Gadzuk, J. W., "Angle Resolved Auger Surface Spectroscopy," *Surface Science*, November 1976, pp. 76–84.
- (32) Tougaard, S., and Hansen, H. S., "Non-Destructive Depth Profiling Through Quantitative Analysis of Surface Electron Spectra," *Surface and Interface Analysis*, Vol 14, 1989, pp. 730–738.

- (33) Veisfeld N., Geller, J.D., "Ion Sputter Yield Measurements for Submicrometer Thin Films," *J. Vac. Sci. Technology*, Vol. 6, 3, II, May/June 1988.
- (34) Chambers, G.P. and Fine J., "Pure Element Sputtering Yield Data," in *Practical Surface Analysis*, Second Edition, Vol. 2, Ion and Neutral

Spectroscopy, edited by D. Briggs and M.P. Seah (John Wiley and Sons, Chichester, 1992), Appendix 4, pp. 704–720.

- (35) International Standards Organization TR 15969 Surface Chemical Analysis—Depth Profiling—Measurement of Sputtered Depth

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