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## What methods exist for calculating the capacity of a shear wall line when there are multiple segments of unequal length?

The American Wood Council’s (AWC) 2015 Special Design Provisions for Wind and Seismic (SDPWS) Section 4.3.3.3.4 provides two options for determining shear distribution to wood-sheathed shear walls in the same line of lateral force resistance when using the segmented shear wall approach. One method is by equal deflection and the other is per distribution of shear in proportion to shear wall length.

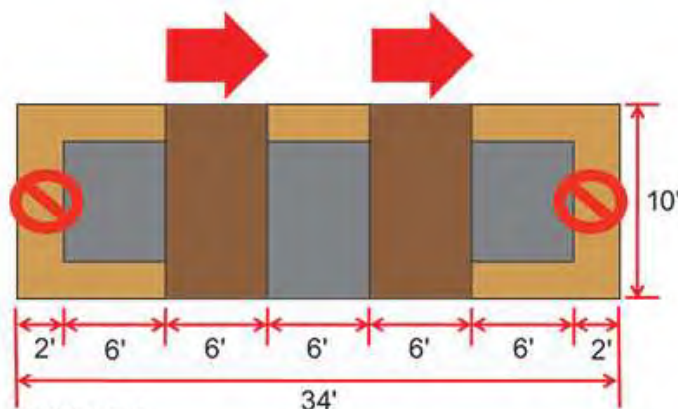
One of the first steps in calculating the capacity for a line of segmented shear walls is to determine which segments in the wall line qualify for use. Table 4.3.4 (Figure 1) gives maximum shear wall aspect ratios for various types of sheathed walls. For blocked wood structural panels, the maximum aspect ratio is 3.5:1. For segments with an aspect ratio between 2:1 and 3.5:1, the nominal shear capacity will need to be multiplied by the Aspect Ratio Factor, which is  $1.25 - 0.125h/b_s$  for wood structural panels (SDPWS 4.3.4.2). Segments with an aspect ratio greater than 3.5:1 cannot be used to resist lateral forces, as shown in Figure 2.

Shear Wall Sheathing Type	Maximum $h/b_s$ Ratio
Wood structural panels, unblocked	2:1
Wood structural panels, blocked	3.5:1
Particleboard, blocked	2:1
Diagonal sheathing, conventional	2:1
Gypsum wallboard	2:1 <sup>a</sup>
Portland cement plaster	2:1 <sup>a</sup>
Structural fiberboard	3.5:1

*a. Walls having aspect ratios exceeding 1.5:1 shall be blocked shear walls.*

**FIGURE 1:**  
SDPWS Table 4.3.4 – Maximum shear wall aspect ratios, courtesy AWC

Where shear wall segments are the same length, simply dividing the total force by the number of segments will provide the force for each one. Unit shear is also easily determined by dividing the total shear force by the sum of resisting segment lengths. From there, the appropriate sheathing, blocking and nailing pattern for the wall can be specified per SDPWS Section 4.3 provisions. For a shear wall line with segments of unequal widths (Figure 3), calculation of the forces to each segment is more involved.



**FIGURE 2:**  
Wall elevation showing qualifying shear wall segments

The Commentary to Chapter 4 of the SDPWS includes two calculation methods for this scenario—the equal deflection method, shown in Example C4.3.3.4.1-1, and the simplified method, illustrated in Example C4.3.3.4.1-2.

### EQUAL DEFLECTION METHOD

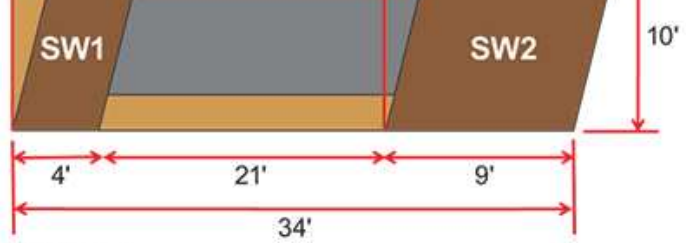
SDPWS 4.3.3.4.1 states that shear distribution to individual shear walls in a shear wall line shall provide the same calculated deflection,  $\delta_{sw}$ , in each shear wall. The equal



deflection method has the basic assumption that the distribution of forces to each wall segment will be based on the relative stiffness of each segment. As the shear wall segments are connected, when the diaphragm transfers shear to the wall line, the segments are assumed to deflect equally.

**Equal Deflection Method**

- $\delta_{SW1} = \delta_{SW2}$



**FIGURE 3:** Shear wall line with segments of unequal lengths shown to deflect equally

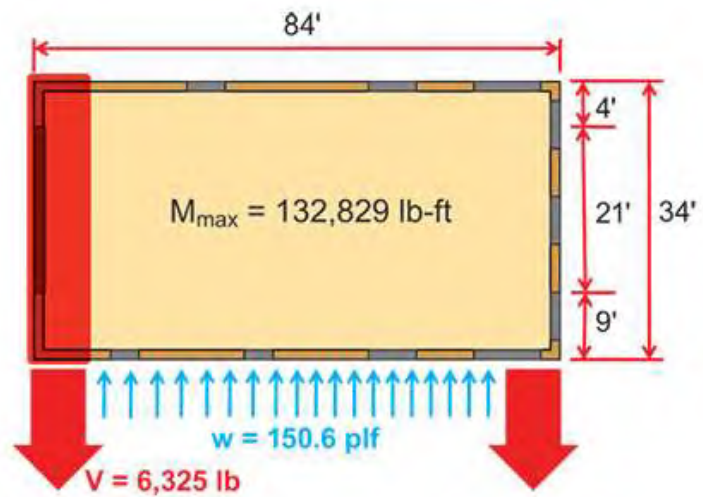
The total design capacity of the shear wall line will be the sum of the resisting forces in each shear wall at the calculated deflection.

As an example, let's consider a building that is 84x34 feet in plan, single story, with 10-foot-tall exterior walls. The first check is to determine the shear wall segment aspect ratios to make sure they fall within the limits detailed in SDPWS Table 4.3.4.

Shear Wall aspect ratios:

SW1 = 10' / 4' = 2.5 < 3.5 OK  
 SW2 = 10' / 9' = 1.1 < 3.5 OK

Checking the ratios, we find that both shear wall segments fall within allowable limits. Also note that the aspect ratio of SW1 is greater than SW2, so its capacity will need to be adjusted per SDPWS 4.3.4.2. Our objective is to calculate the maximum wall strength (capacity) based on the maximum nominal shears for the wall construction, which can then be compared to actual demand.



**FIGURE 4:** Shear wall line with segments of unequal lengths shown to deflect equally

For shear wall design in this example, we assume 15/32-inch OSB, Wood Structural Panels – Sheathing, attached with 8d nails @ 3 inches on center to 2x6 Spruce Pine Fir (SPF) framing spaced 16 inches on center with two 2x6 posts at the end of each wall segment. Forces from wind loading are shown in Figure 4. The wall line in question is the left wall on the plan shown in Figure 4 (elevation view shown in Figure 3).

**SW1**

$h/b_s = 2.5 > 2$

Aspect Ratio Factor =  $1.25 - 0.125(h/b_s) = 0.938$  (SDPWS Section 4.3.4.2)

From SDPWS Table 4.3A:

Nominal unit shear capacity = 1,370 lb/ft

Adjusted ASD capacity =  $[(1,370 \text{ plf})(0.92)/2] * 0.938 = 591 \text{ lb/ft}$

0.92 is the adjustment for having SPF framing; see SDPWS Table 4.3A, footnote 3. Divide by 2 for the ASD allowable unit shear capacity per SDPWS 4.3.3.

**SW2**

As our sheathing thickness, blocking and nailing pattern will remain the same for both segments, by observation we recognize that SW2 is the stiffer of the two shear wall segments (longer). SW2 will have the smaller deflection at its capacity and ultimately control the deflection of both shear walls.

$h/b_s = 1.11 < 2$  OK

Nominal unit shear capacity = 1,370 lb/ft (SDPWS Table 4.3A)

Adjusted ASD capacity = (1,370 plf)(0.92)/2 = 630 lb/ft

We now calculate the deflection of SW2 at its ASD unit shear capacity:

(bending) (shear) (wall anchorage slip)

$$\delta_{sw} = \frac{8vh^3}{EAb} + \frac{vh}{1000G_a} + \frac{h}{b} \Delta_a \quad (C4.3.2-2)$$

v = 630 lb/ft

E = 1,400,000 psi (NDS\* Supplement Table 4A)

A = 2(1.5"x5.5") = 16.5 in<sup>2</sup> (2-2x6 stud end post)

b = 9'

h = 10'

G<sub>a</sub> = 14 k/in (SDPWS Table 4.3A)

Δ<sub>a</sub> = vertical elongation of wall anchorage = 0.091" at 6,560 lbs (from hold down manufacturer)

SW2 anchorage force = (630 lb/ft)(10') = 6,300 lb

\*Assuming vertical elongation is linear, we can calculate elongation for our load of 6,300 lbs.

Δ<sub>a</sub> = 6,300 \* 0.091" / 6,560 lb = 0.087"

δ<sub>SW2</sub> = 0.571"

Determine the unit shear in SW1 that produces the same deflection as SW2:

k = stiffness of the anchorage = F / d (deflection / elongation)

k = 6,560 lbs / 0.091" = 72,087 lb/in

$$v_{SW1} = \frac{\delta}{\frac{8h^3}{EAb_{SW1}} + \frac{h}{1000G_a} + \frac{h^2}{kb_{SW1}}}$$

$$v_{SW1} = \frac{0.45''}{\frac{8(10')^3}{(1,400,000)(16.5)(4')} + \frac{(10')}{1000(14,000)} + \frac{(10')^2}{(72,087)(4')}} = 497 \text{ lb/ft}$$

v<sub>SW1</sub> = 497 lb/ft < 591 lb/ft

Shear wall line capacity:

V = (497 lb/ft)\*4' + (630 lb/ft)\*9'

V = 1,988 lbs + 5,670 lbs

V = 7,658 lb > 6,325 lb Actual OK

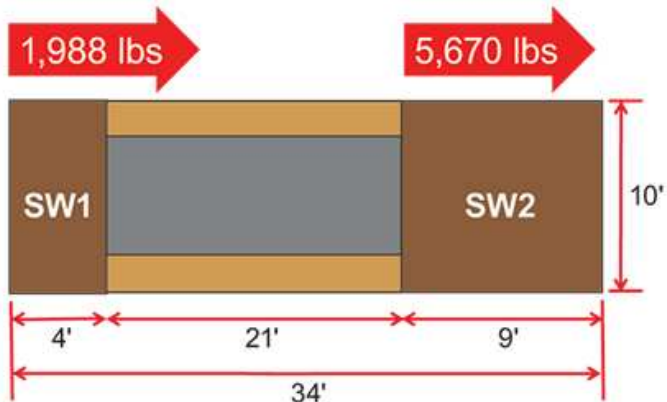


FIGURE 5: Resultant forces on shear wall segments using the equal deflection method

SIMPLIFIED METHOD

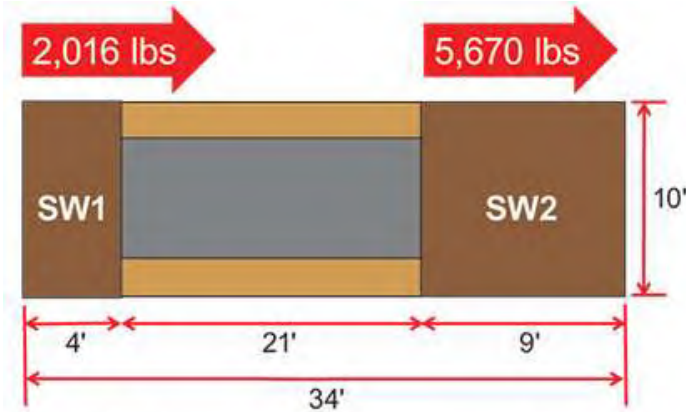
For wood structural panels, distribution of shear in proportion to shear strength (by wall length) of each shear wall is

permitted provided shear walls with aspect ratios greater than 2:1 have strength adjusted by the  $2b_s/h$  factor (per 2015 SDPWS 4.3.3.4.1, Exception 1). Using this method:

SW1  
 SW1 Aspect Ratio = 2.5 > 2 Nominal shear capacity will need to be adjusted by  $2b_s/h$  per SDPWS 4.3.3.4.1 Exception 1.  
 $h/b_s = 2.5 > 2$   
 $2b_s/h = 2*(4'/10') = 0.8$   
 Nominal unit shear capacity = 1,370 lb/ft (SDPWS Table 4.3A)  
 Adjusted ASD capacity =  $[(1,370 \text{ plf})(0.92)/2]*0.8 = 504 \text{ lb/ft}$

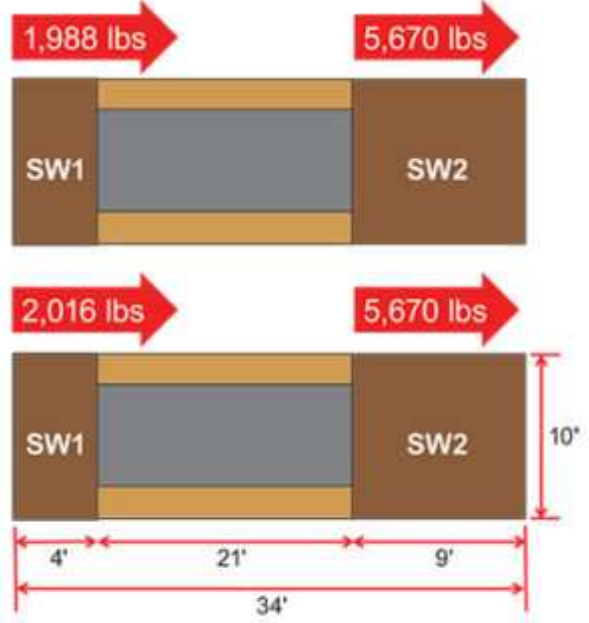
SW2  
 $h/b_s = 1.1 < 2$   
 Nominal unit shear capacity = 1,370 lb/ft (SDPWS Table 4.3A)  
 Adjusted ASD capacity =  $(1,370 \text{ plf})(0.92)/2 = 630 \text{ lb/ft}$

Shear wall line capacity:  
 $V = (504 \text{ lb/ft}) * 4' + (630 \text{ lb/ft}) * 9'$   
 $V = 2,016 \text{ lbs} + 5,670 \text{ lbs}$   
 $V = 7,686 \text{ lb} > 6,325 \text{ lb Actual OK}$



**FIGURE 6:**  
 Resultant forces on shear wall segments using the simplified method

Comparing the two methods we see a slight increase in the resistance provided by the simplified method.



**FIGURE 7:**  
 Equal Deflection Method (top) and Simplified Method (bottom)

Beyond the segmented shear wall approach, SDPWS Section 4.3.5 describes two other methods for evaluating shear wall lateral resistance—the Perforated Shear Wall (PSW) method and Force Transfer Around Openings (FTAO) method. For further reading on these two methods, see the resources listed below.

\*National Design Specification® (NDS®) for Wood Construction, AWC

## Additional Resources:

- [Diaphragms and Shear Walls](#), APA – The Engineered Wood Association (APA)
- [APA Wall Bracing Calculator](#), APA
- [Wind Solutions – Perforated Wood Structural Panel Shear Walls](#), AWC
- [Technical Note: Design for Force Transfer Around Openings](#), APA
- [APA Force Transfer Around Openings Calculator](#), APA
- [Wood-Framed Shear Walls – Utilizing Force Transfer Around Openings](#), Hensley, J., APA, Structure magazine
- [When designing light wood-frame shear walls with openings and using the force transfer around openings \(FTAO\) method, do the metal straps along the tops and bottoms of the openings need to extend the full wall length?](#), WoodWorks Ask an Expert
- [Shear Walls Design Examples](#), AWC

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