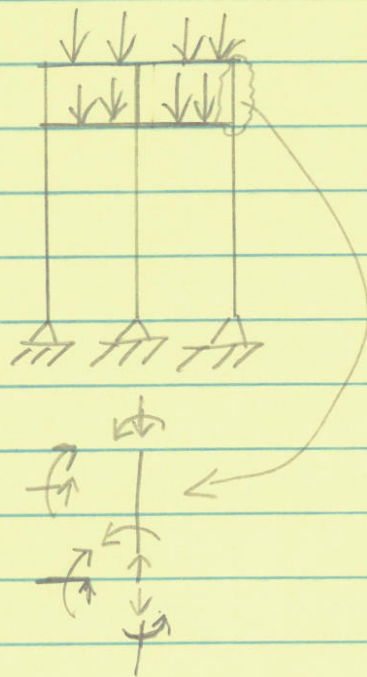


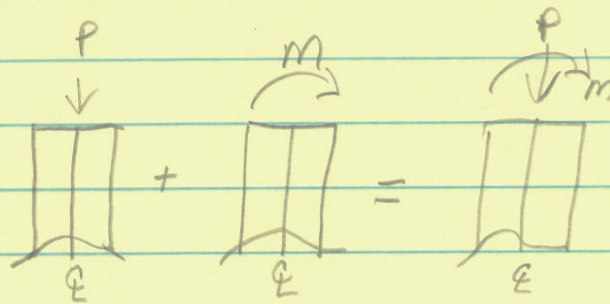
Columns



Columns
 Interactions
 Concrete Reality
 Interaction
 diagram
 Example
 Slenderness
 Sway
 Design

Wed 10-20 Review
 Mon 10-25 ACI
 Wed 10-27 Exam

Stresses in Normal Columns



$$f + \frac{P}{A} + \frac{Mc}{I} = f + \frac{P}{A} + \frac{Mc}{I}$$

The diagram shows the stress distribution in a column under axial load and bending moment. The stress is f at the neutral axis. The axial load P adds a uniform stress P/A . The bending moment M adds a linear stress distribution Mc/I .

P & M Interact to determine f

Interaction Equations
 Assume linear Elastic homogeneous prismatic

$$\frac{P}{A} + \frac{Mc}{I} \leq F_{max} \quad (\text{some max stress levels})$$

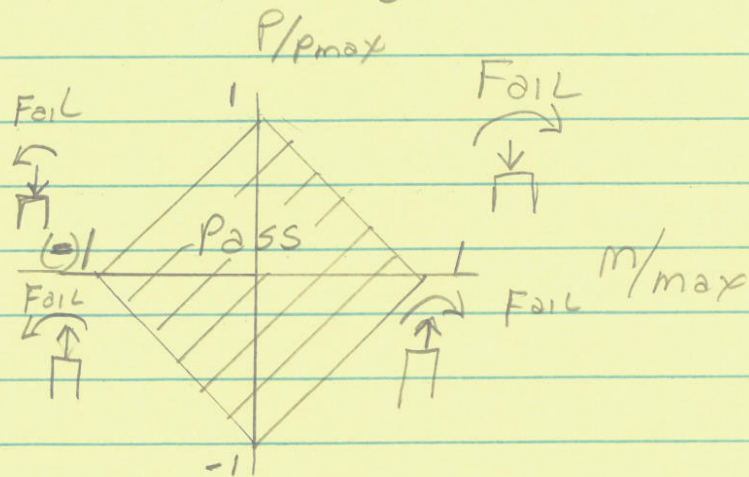
divide by F_{max}

$$\frac{P}{A F_{max}} + \frac{Mc}{I F_{max}} \leq 1.0$$

$$\frac{P_{max}}{A} \quad \frac{m_{max} c}{I}$$

$$\frac{P}{P_{max}} + \frac{m}{m_{max}} \leq 1.0$$

Interaction Diagram



Assuming $F_{max t} = F_{max c}$

Back to Reality

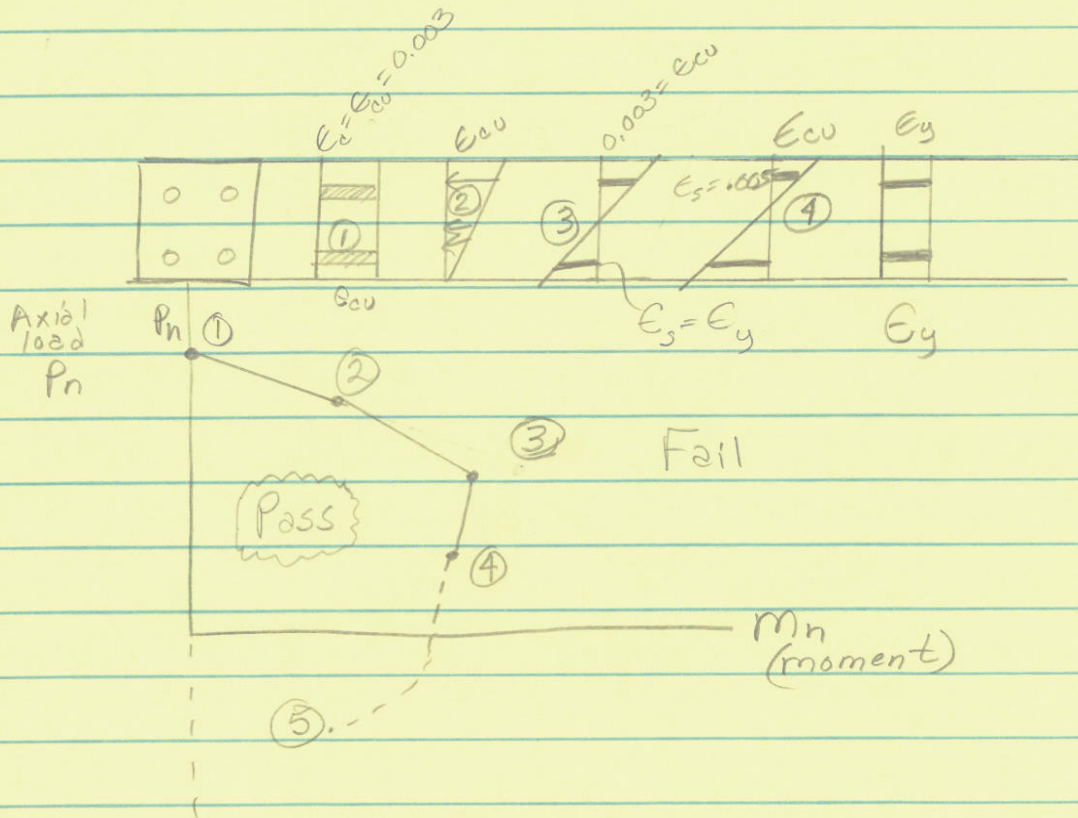
RC is not homogenous

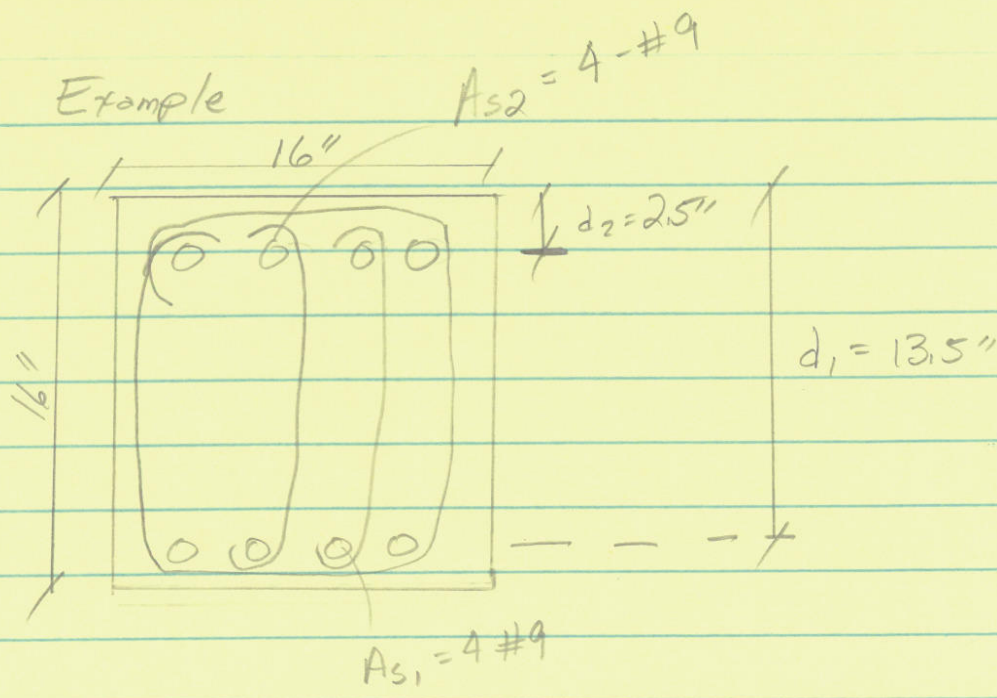
RC Simplified Interaction Diagram

Build w/5 key points

$\epsilon_{cu} = 0.003$
concrete ultimate

- ① Uniform compression $\epsilon_c = \epsilon_{cu}$
- ② $\epsilon_{top} = \epsilon_{cu}$, $\epsilon_{bottom} = 0$
- ③ Balanced: $\epsilon_{top} = \epsilon_{cu}$, $\epsilon_s = \epsilon_y$
- ④ $\epsilon_{top} = \epsilon_{cu}$, $\epsilon = 0.005$
- ⑤ Uniform tensile strain $\epsilon = \epsilon_y$





Compute 4 points on the interaction diagram

$$f'_c = 5 \text{ ksi}$$

$$f_y = 60 \text{ ksi}$$

gross Area bh $A_g = bh = 256 \text{ in}^2$

$$A_{s1} = 4 \text{ in}^2$$

$$A_{s2} = 4 \text{ in}^2$$

$$A_{sT} = 8 \text{ in}^2$$

$$I_{sT} = \frac{A_{sT}}{A_g} = 0.031$$

Point 1 uniform compression

$$\epsilon_c = \epsilon_{cu} = 0.003 \quad \epsilon_s = 0.00376_y$$

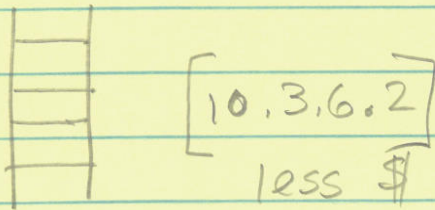
Columns with spirals Reinforcement



[10.3.6.1]
more \$

Better in seismic regions

Columns with Tie Reinforcement



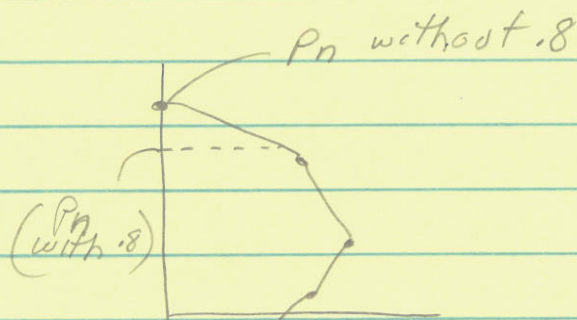
$$\phi P_n = 0.80 \phi [0.85 F'_c (A_g - A_{st}) + f_y A_s]$$

$$\phi = 0.65 \cdot [9.3.2.2] \text{ compression + tied } \left. \begin{array}{l} \text{concrete} \\ \text{steel} \end{array} \right\}$$

$$= 0.80 \phi [0.85(5000)(256 - 8) + 60,000(8)]$$

$$P_n = 1534 \text{ kips}$$

$$\phi P_n = 997 \text{ kips}$$



ϕ Factors

IAD point

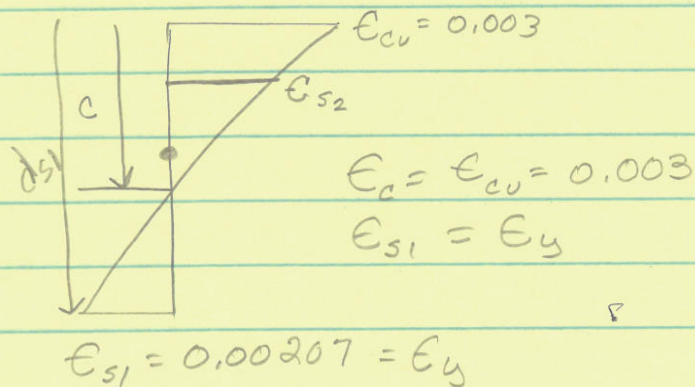
- 1
 - 2
 - 3
 - 4
 - 5
- Compression
TIED
Transition [R9.3.2]
Tension

ϕ

TIED = 0.65
SPIRAL = 0.70

0.9

Pt 2,3,4
Point 3 balanced



determine NA Neutral Axis

$$\frac{\epsilon_{cu}}{c} = \frac{\epsilon_{s1} + \epsilon_{cu}}{ds_1}$$

$$c = \frac{\epsilon_{cu} ds_1}{\epsilon_{s1} + \epsilon_{cu}} = \frac{0.003 (13.5)}{0.0027 + 0.003}$$

$$c = 7.99 \text{ in}$$

determine force resultants

$$a = \beta_1 c = 0.8 (7.99) = 6.39 \text{ in}$$

(if $a > h$, use h)

Compression
Steel

$$C_c = 0.85 f'_c a b = 0$$

$$= 4.34.6 \text{ k}$$

$$T_s = f_{s1} A_s = -60 (4) = -240 \text{ k}$$

$$C_s = (f_{s2} - 0.85 f'_c) A_{s2}$$

$$C_s = (59.8 - 0.85 (6 \text{ ksi})) (4) = 221 \text{ k}$$

calculate ϵ_{s2} then
calc f_{s2}

Calculate P_n M_n

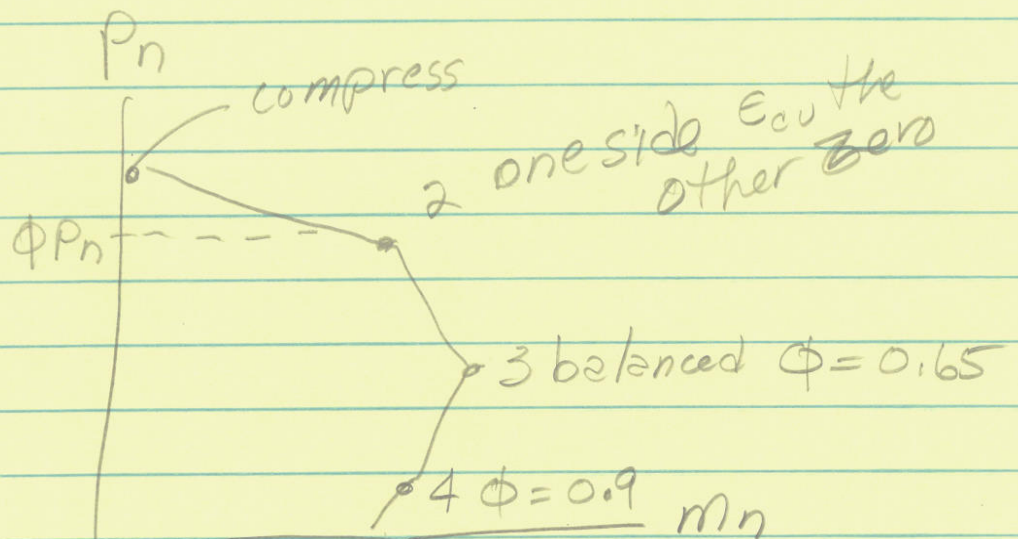
$$P_n = C_c + \sum F_{s2} = 434.6 + 222.1 - 24$$

$$P_n = 417 \text{ k}$$

$\sum M$ @ centroid

$$M_n = C_c \left(\frac{h}{2} - \frac{a}{2} \right) + F_{s1} \left(\frac{h}{2} - d_1 \right) + F_{s2} \left(\frac{h}{2} - d_2 \right)$$

$$(P_n, M_n)_3 = (417, 4630)$$



5 ALL tension

$$P_n = A_s f_y$$