

Steam Quality Problems:

Find the steam quality for the following problems.

- (a) H_2O ; $T = 20^\circ\text{C}$, $v = 20 \text{ m}^3/\text{kg}$,
 From Table A-2, $v_f = 1.0018 \times 10^{-3} \text{ m}^3/\text{kg}$, $v_g = 57.791 \text{ m}^3/\text{kg}$

$$\text{So, } x = \frac{v - v_f}{v_g - v_f} = \frac{20 - 1.0018 \times 10^{-3}}{57.791 - 1.0018 \times 10^{-3}} = 0.346 = 34.6\%$$
- (b) C_3H_8 ; $P = 15.00 \text{ bar}$, $v = 0.02997 \text{ m}^3/\text{kg}$, From Table A-17, $v_g = 0.02997 \text{ m}^3/\text{kg}$

$$\text{So, } x = 1 = 100\%$$
- (c) Refrigerant 134a; $T = 60^\circ\text{C}$, $v = 0.001 \text{ m}^3/\text{kg}$
 From Table A-10, $v_f = 0.9488 \times 10^{-3} \text{ m}^3/\text{kg}$, $v_g = 0.0114 \text{ m}^3/\text{kg}$

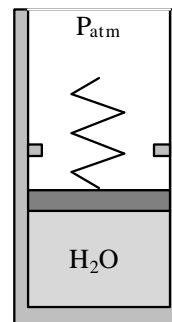
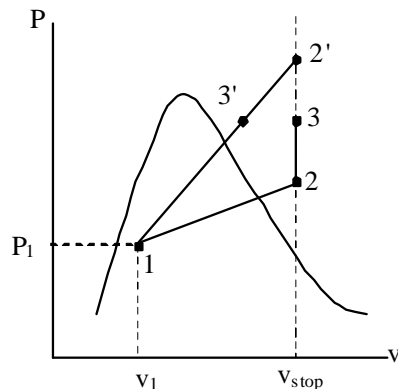
$$\text{So, } x = \frac{v - v_f}{v_g - v_f} = \frac{0.001 - 0.9488 \times 10^{-3}}{0.0114 - 0.9488 \times 10^{-3}} = 0.0049 = 0.49\%$$
- (d) NH_3 ; $P = 1 \text{ MPa} = 10 \text{ bar}$, $v = 0.1 \text{ m}^3/\text{kg}$
 From Table A-14, $v_f = 1.6584 \times 10^{-3} \text{ m}^3/\text{kg}$, $v_g = 0.1285 \text{ m}^3/\text{kg}$

$$\text{So, } x = \frac{v - v_f}{v_g - v_f} = \frac{0.1 - 1.6584 \times 10^{-3}}{0.1285 - 1.6584 \times 10^{-3}} = 0.775 = 77.5\%$$

4.110 Book-Borgnakke

2 kg of water is contained in a piston/cylinder (Figure) with a mass less piston loaded with a linear spring and the outside atmosphere. Initially the spring force is zero and $P_1 = P_0 = 100 \text{ kPa}$ with a volume of 0.2 m^3 . If the piston just hits the upper stops the volume is 0.8 m^3 and $T = 600^\circ\text{C}$. Heat is now added until the pressure reaches 1.2 MPa . Find the final temperature, show the P-v diagram and find the work done during the process.

Sol. Schematic



State 1: $v_1 = \mathcal{V}/m = 0.2/2 = 0.1 \text{ m}^3/\text{kg}$

Process: 1-2-3 or 1-3'

State at stops: 2 or 2'; $v_2 = \mathcal{V}_{\text{stop}}/m = 0.8/2 = 0.4 \text{ m}^3/\text{kg}$ and $T_2 = 600^\circ\text{C}$, $P_2 \approx 1000 \text{ kPa}$

Table A-4, $P_{\text{stop}} < 1 \text{ MPa} < P_3$. Since $T_{\text{stop}} < P_3$ the process is as 1-2-3

State 3: $P_3 = 1.2 \text{ MPa}$, $v_3 = v_2 = 0.4 \text{ m}^3/\text{kg}$,

$$\text{So, } \frac{T_3 - 700}{800 - 700} = \frac{0.4 - 0.37294}{0.41177 - 0.37294} \Rightarrow T_3 = 769.7^\circ\text{C}$$

$$W_{13} = W_{12} + W_{23} = \frac{1}{2} (P_1 + P_2) (\mathcal{V}_2 - \mathcal{V}_1) + 0 = \frac{1}{2} (100 + 1000) (0.8 - 0.2) = 330 \text{ kJ}$$

5.73 A cylinder/piston arrangement contains 5 kg of water at 100°C with $x = 20\%$ and the piston, $m_p = 75\text{kg}$, resting on some stops like the figure. The outside pressure is 100 kPa and the cylinder area is $A = 24.5\text{ cm}^2$. Heat is now added until the water reaches a saturated vapor state. Find the initial volume, final pressure, work and heat transfer terms and show the P-v diagram.

Sol. C.V. the 5 kg water.

Mass conservation, $m_1 = m_2 = m$

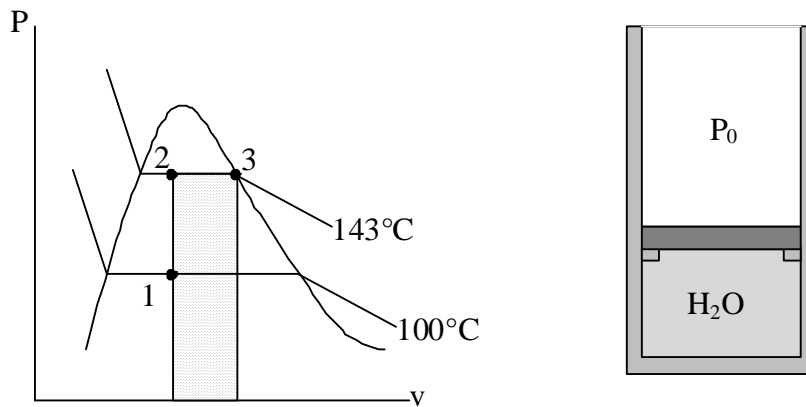
Energy conservation, $m(u_2 - u_1) = {}_1Q_2 - {}_1W_2$

Process: $V = \text{Constant}$ if $P < P_{\text{lift}}$ otherwise $P = P_{\text{lift}}$ in P-v diagram

$$P_3 = P_2 = P_{\text{lift}} = P_0 + \frac{m_p g}{A_p} = 100 + \frac{75 \times 9.807}{0.00245 \times 1000} = 400\text{kPa}$$

At 100°C, 101.3 kPa, $v_g = 1.6729\text{ m}^3/\text{kg}$. If all H₂O becomes vapor, the volume would be, $V = m v_g = 5 \times 1.6729 = 8.3645\text{ m}^3 > V_1$,

So, $P_3 > P_1$ and the heating process must go through isometric process first with increased pressure until $P = P_{\text{lift}}$.



State 1: For $T_1 = 100^\circ\text{C}$ and $x = 0.2$, from Table A-2,
 $v_1 = 0.001035 + 0.2 \times 1.6719 = 0.3354\text{ m}^3/\text{kg}$, $V_1 = m v_1 = 5 \times 0.3354 = 1.677\text{ m}^3$
 $u_1 = 418.94 + 0.2 \times (2506.5 - 418.94) = 836.4\text{ kJ/kg}$

State 3: For $P_3 = 400\text{kPa}$ and $x = 1$, from Table A-3,
 $v_3 = v_{3g} = 0.4625\text{ m}^3/\text{kg} > v_1$, $u_3 = u_{3g} = 2553.6\text{ kJ/kg}$

Work is seen in P-v diagram (if volume changes then $P = P_{\text{lift}}$)

$${}_1W_3 = {}_2W_3 = P_{\text{ext}} m (v_3 - v_2) = 400 \times 5 \times (0.46246 - 0.3354) = 254.1\text{ kJ}$$

Heat transfer is from the energy equation,

$${}_1Q_2 = m(u_2 - u_1) + {}_1W_2 = 5 \times (2553.6 - 836.4) + 254.1 = 8840\text{ kJ}$$

4.111 Book-Borgnakke

A cylinder having an initial volume of 3m^3 contains 0.1 kg of water at 40°C . The water is then compressed in an isothermal quasi-equilibrium process until it has a quality of 50% . Calculate the work done and heat input in the process splitting it into two steps. Assume the water vapor in an ideal gas during the first step of the process.

Sol. C.V. Water.

State 2: 40°C and $x = 1$, from Table A-2, we get, $P_{\text{sat}} = 7.384\text{ kPa}$, $v_g = 19.523\text{ m}^3/\text{kg}$

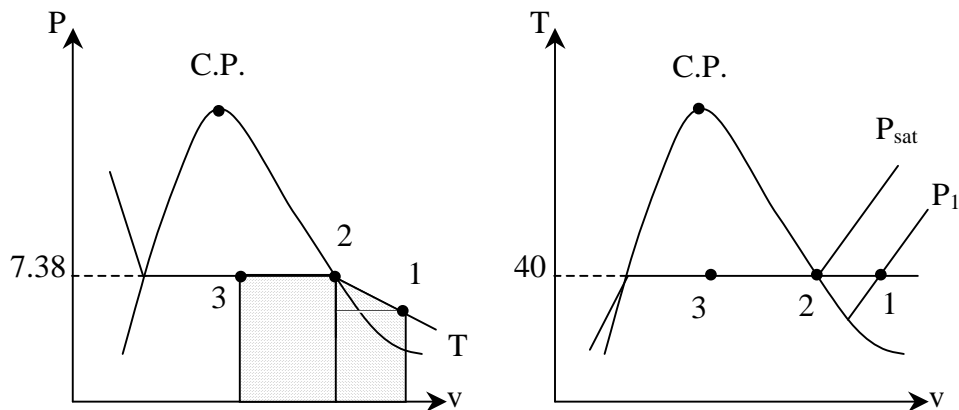
State 1: $v_1 = V_1/m = 3/0.1 = 30\text{ m}^3/\text{kg} > v_g$. (So superheated, $u_1 = 2430\text{ kJ/kg}$)

So, H_2O as an ideal gas (in superheated state),

From 1-2 through isothermal process ($Pv = \text{Constant}$)

$$P_1 = P_{\text{Sat}} v_g/v_1 = 7.384 \times 19.523 / 30 = 4.8\text{ kPa}$$

$$V_2 = m v_2 = 0.1 \times 19.523 = 1.952\text{ m}^3$$



Process, $T = C$: and ideal gas gives work,

$$W_{12} = \int_1^2 PdV = P_1 v_1 \ln\left(\frac{v_2}{v_1}\right) = 4.8 \times 3.0 \times \ln\left(\frac{1.952}{3}\right) = -6.19\text{ kJ}$$

State 3: $T_3 = T_2 = T_1 = 40^\circ\text{C}$

$$v_3 = 0.0010078 + 0.5 \times (15.523 - 0.0010078) = 9.7605\text{ m}^3/\text{kg}, \text{ so, } V_3 = m v_3 = 0.976\text{ m}^3$$

$$u_3 = 167.56 + 0.5 \times (2430 - 167.56) = 1298.83\text{ kJ/kg}$$

$P = P_{\text{Sat}} = \text{Constant}$: This give a work term as,

$$W_{23} = \int_2^3 PdV = P_{\text{Sat}} (v_3 - v_2) = 7.384 \times (0.976 - 1.952) = -7.21\text{ kJ}$$

$$\text{So, total work, } W_{13} = W_{12} + W_{23} = -6.19 - 7.21 = -13.4\text{ kJ/kg}$$

First law,

$$Q_{\text{in}} = W_{\text{out}} + m(u_3 - u_1) = -13.4 + 0.1 \times (1298.83 - 2430) = -126.517\text{ kJ (cooling)}$$

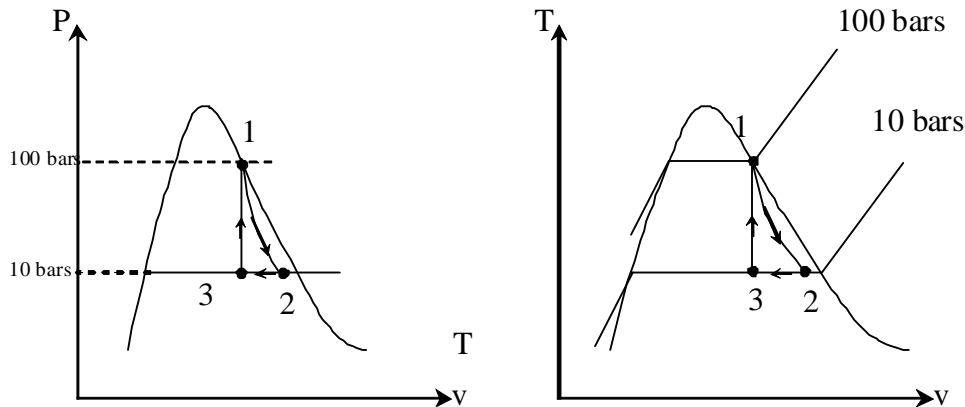
Known: A system consisting of H₂O undergoes a cycle composed of three processes. Sketch P-v and T-v diagrams. Determine the cycle net work and the heat transfer for each process.

Schematic and given data: The following data are given for each process.

Process 1-2: Expansion with $Pv = \text{Constant}$ from saturated vapor at 100 bars to 10 bars

Process 2-3: Isobaric process $v_3 = v_1$

Process 3-1: Isometric heating



Assumptions: (i) Closed system
(ii) Neglect KE and PE.

Analysis: First, using data from Table A-2, fix each state.

State 1: $P_1 = 100 \text{ bar}$, sat. vapor, thus $v_1 = v_g = 0.01803 \text{ m}^3/\text{kg}$, $u_1 = u_g = 2544.4 \text{ kJ/kg}$

State 2: From $Pv = \text{Constant}$, $v_2 = (P_1 v_1)/P_2 = 0.1803 \text{ m}^3/\text{kg}$,

This state is a two-phase state, so for $v_2 = 0.1803 \text{ m}^3/\text{kg}$, $u_2 = 2450.7 \text{ kJ/kg}$

State 3: $v_3 = v_1 = 0.01803 \text{ m}^3/\text{kg}$, so for $v_3 = 0.01803 \text{ m}^3/\text{kg}$, $u_3 = 921.0 \text{ kJ/kg}$

Now, the work for each states.

$$W_{12} = mP_1 v_1 \ln\left(\frac{v_2}{v_1}\right) = 2 \times 100 \times 10^2 \times 0.01803 \times \ln\left(\frac{0.1803}{0.01803}\right) = 830.3 \text{ kJ}$$

$$W_{23} = mP_2 (v_3 - v_2) = 2 \times 100 \times 10^2 \times (0.1803 - 0.01803) = -324.5 \text{ kJ}$$

$$W_{31} = 0 \text{ (as isometric process and closed system)}$$

$$\text{So, the net work is, } W_{\text{cycle}} = W_{12} + W_{23} + W_{31} = 830.3 - 324.5 + 0 = 505.8 \text{ kJ}$$

The heat transfer for each process can be found out as,

$$Q_{12} = m (u_2 - u_1) + W_{12} = 2 \times (2450.7 - 2544.4) + 830.3 = 642.9 \text{ kJ}$$

$$Q_{23} = m (u_3 - u_2) + W_{23} = 2 \times (921.0 - 2450.7) - 324.5 = -3383.9 \text{ kJ}$$

$$Q_{31} = m (u_1 - u_3) + W_{31} = 2 \times (2544.4 - 921.0) + 0 = 3246.8 \text{ kJ}$$

Comment: $Q_{\text{cycle}} = Q_{12} + Q_{23} + Q_{31} = 642.9 - 3383.9 + 3246.8 = 505.8 \text{ kJ}$

So, $W_{\text{cycle}} = Q_{\text{cycle}}$ as expected.

Prepared by: Jobaidur Rahman Khan

Known: Ethylene is compressed isobarically from $P_1 = 213$ Psia, $T_1 = 612^\circ\text{R}$ to $T_2 = 460^\circ\text{R}$.
Determine the work per mole of ethylene.

Given data: $P_1 = P_2 = 213$ lbf/in², $T_1 = 612^\circ\text{R}$, $T_2 = 460^\circ\text{R}$

Assumptions: (i) The ethylene is in a closed system
(ii) The process is isobaric.
(iii) Negligible KE and PE.

Analysis: The work is evaluated as, $W = nP(\bar{v}_2 - \bar{v}_1) \Rightarrow \frac{W}{n} = P(\bar{v}_2 - \bar{v}_1)$

The work is determine after \bar{v}_1 and \bar{v}_2 are found. First, using the data from Table A-1E.
 $P_c = 50.5$ bars, $T_c = 510^\circ\text{R}$

So, $P_{R1} = P_1/P_c = 213/(50.5 \times 14.7) = 0.287$

$T_{R1} = T_1/T_c = 612 / 510 = 1.2$

And from Fig. A-1E, $v'_{R1} = 4.00$

$$\text{Thus, } \bar{v}_1 = v'_{R1} \left(\frac{\bar{R}T_c}{P_c} \right) = 4.00 \times \frac{\left(1545 \frac{\text{ft.lbf}}{\text{lbmole.}^\circ\text{R}} \right) \times (510^\circ\text{R})}{(50.5 \times 14.7) \frac{\text{lbf}}{\text{in}^2}} \left(\frac{1\text{ft}^2}{144\text{in}^2} \right) = 29.48\text{ft}^3/\text{lbmole}$$

Again, $P_{R2} = P_{R1} = 0.287$

$T_{R2} = T_2/T_c = 460 / 510 = 0.9$

And from Fig. A-1E, $v'_{R2} = 2.62$

$$\text{Thus, } \bar{v}_2 = v'_{R2} \left(\frac{\bar{R}T_c}{P_c} \right) = 2.62 \times \frac{\left(1545 \frac{\text{ft.lbf}}{\text{lbmole.}^\circ\text{R}} \right) \times (510^\circ\text{R})}{(50.5 \times 14.7) \frac{\text{lbf}}{\text{in}^2}} \left(\frac{1\text{ft}^2}{144\text{in}^2} \right) = 19.31\text{ft}^3/\text{lbmole}$$

Finally the work,

$$\frac{W}{n} = \left(213 \frac{\text{lbf}}{\text{in}^2} \right) \left(\frac{1\text{in}^2}{144\text{ft}^2} \right) (19.31 - 29.48) \frac{\text{ft}^3}{\text{lbmole}} \left(\frac{1\text{Btu}}{778\text{ft.lbf}} \right) = -400.9\text{Btu} / \text{lbmole}$$

Comment: The work for the compression process is negative, as expected.