



Standard Practice for Measuring Trace Elements in Water by Graphite Furnace Atomic Absorption Spectrophotometry¹

This standard is issued under the fixed designation D 3919; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

1. Scope*

1.1 This practice covers the general considerations for the quantitative determination of trace elements in water and wastewater by graphite furnace atomic absorption spectrophotometry. Furnace atomizers are a most useful means of extending detection limits; however, the practice should only be used at concentration levels below the optimum range of direct flame aspiration atomic absorption spectrophotometry. Because of differences between various makes and models of satisfactory instruments, no detailed operating instructions can be provided for each instrument. Instead, the analyst should follow the instructions provided by the manufacturer of a particular instrument.

1.2 Wavelengths, estimated detection limits, and optimum concentration ranges are given in the individual methods. Ranges may be increased or decreased by varying the volume of sample injected or the instrumental settings or by the use of a secondary wavelength. Samples containing concentrations higher than those given in the optimum range may be diluted or analyzed by other techniques.

1.3 This technique is generally not applicable to brines and seawater. Special techniques such as separation of the trace elements from the salt, careful temperature control through ramping techniques, or matrix modification may be useful for these samples.

1.4 The analyst is encouraged to consult the literature as provided by the instrument manufacturer as well as various trade journals and scientific publications.

1.5 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Referenced Documents

2.1 ASTM Standards:²

- D 1129 Terminology Relating to Water
- D 1192 Specification for Equipment for Sampling Water and Steam in Closed Conduits
- D 1193 Specification for Reagent Water
- D 2777 Practice for Determination of Precision and Bias of Applicable Methods of Committee D19 on Water
- D 3370 Practices for Sampling Water from Closed Conduits
- D 4841 Practice for Estimation of Holding Time for Water Samples Containing Organic and Inorganic Constituents
- D 5810 Guide for Spiking into Aqueous Samples
- D 5847 Practice for Writing Quality Control Specifications for Standard Test Methods for Water Analysis

3. Terminology

3.1 *Definitions*—For definitions of terms used in this practice, refer to Terminology D 1129.

3.2 *Definitions of Terms Specific to This Standard:*

3.2.1 *graphite furnace*—an electrothermal graphite device capable of reaching the specified temperatures required by the element being determined.

3.2.2 *platform or similar device*—a flat, grooved or ungrooved piece of pyrolytic graphite inserted in the graphite tube on which the sample is placed **(1)**.³

4. Summary of Practice

4.1 The element is determined by an atomic absorption spectrophotometer used in conjunction with a graphite furnace. The principle is essentially the same as with direct flame aspiration atomic absorption except a furnace, rather than a flame, is used to atomize the sample. The elemental atoms to be measured are placed in the beam of radiation by increasing the

¹ This practice is under the jurisdiction of ASTM Committee D19 on Water and is the direct responsibility of Subcommittee D19.05 on Inorganic Constituents in Water.

Current edition approved March 1, 2004. Published April 2004. Originally approved in 1980. Last previous edition approved in 1999 as D 3919 – 99.

² For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For Annual Book of ASTM Standards volume information, refer to the standard's Document Summary page on the ASTM website.

³ The boldface numbers in parentheses refer to the list of references at the end of this standard.

temperature of the furnace, thereby causing the injected specimen to be volatilized. Radiation from a given excited element is passed through the vapor containing ground-state atoms of that element. The decrease in intensity of the transmitted radiation is a measure of the amount of the ground-state element in the vapor. A monochromator isolates the characteristic radiation from the hollow-cathode lamp and a photosensitive device measures the attenuated transmitted radiation.

4.2 Dissolved elements are determined on a filtered sample with no pretreatment. See 9.5.

4.3 Total recoverable elements are determined following acid digestion and filtration. If suspended material is not present, this digestion and filtration may be omitted.

5. Significance and Use

5.1 Elemental constituents in potable water, receiving water, and wastewater need to be identified for support of effective pollution control programs. Currently, one of the most sensitive and practical means for measuring low concentrations of trace elements is by graphite furnace atomic absorption spectrophotometry.

6. Interferences

6.1 Background absorption is caused by the formation of molecular species from the sample matrix that absorb or scatter the light emitted by the hollow cathode or electrodeless discharge line source. Without correction, this will cause the analytical results to be erroneously high. Three approaches exist for simultaneous background correction: continuum source, Zeeman, and Smith-Hieftje.

6.1.1 *Continuum Source*—The continuum source procedure involves the use of a deuterium arc source for the ultraviolet or a tungsten halide lamp for the visible region of the spectrum. Light from the primary spectral source and the appropriate continuum source are alternately passed through the graphite furnace. Narrow-band emission of the primary source is affected by the scatter and background absorption from the matrix as well as the absorption of light by analyte atoms. The broadband emission of the continuum source is affected only by the background absorption. The effect of the background is removed by taking a ratio of the energy of the two sources.

6.1.2 *Zeeman Correction*—The Zeeman correction system involves the use of an external magnetic field to split the atomic spectral line. When the magnetic field is off, both sample and background are measured. When the magnetic field is applied, the absorption line is shifted and only the background absorption is measured. Background correction is performed by electronically comparing the field-off and field-on measurements, yielding an analyte-only absorption response.

6.1.3 *Smith-Hieftje System*—This system involves cycling the atomic line source at high currents for brief intervals. These intervals cause nonexcited atoms of the source element to undergo the process of self-reversal by emitting light at wavelengths other than those of the analyte. This light is absorbed only by the background, so that interspersing periods of high and low source current permit correction of the background.

6.2 Some types of interference problems encountered in direct aspiration atomic absorption spectrophotometry can be observed with the furnace technique. Although quite rare, spectral interference may be encountered. When this occurs, the use of another wavelength is suggested. Additionally, the furnace technique is subject to chemical and matrix interference and the composition of the sample matrix can have a major effect on the analysis. Therefore, for each different matrix encountered, the possibility of these interferences should be considered. The tests as outlined in 6.2.1-6.2.5 are recommended prior to reporting analytical data. These tests will provide indication whether positive or negative interference effects are operative in any way on the analyte elements thereby distorting the accuracy of the reported values.

6.2.1 *Spiking Verification*—When the sample absorbance is 40 % or less of the absorbance of the highest standard on the standard curve, the amount of spike added to the sample should result in a net increase equal to 50 % of the highest standard concentration. The purpose of adding a large spike is to differentiate between matrix interferences and random errors. The recovery of the spike must be between 90 and 110 % for verification of the original determination. If the result of the original determination is above 40 % on the curve, two aliquots should be withdrawn and diluted at least 1 + 1. One of the aliquots should be spiked before dilution with an amount resulting in a net increase over the unspiked aliquot equivalent to 50 % of the highest standard concentration. The reported result should be based on the analysis of the diluted aliquot. For verification of this result, the spike recovery must be between 90 and 110 %. For spiking verification to be valid in either situation in the presence of nonspecific absorbance, simultaneous background correction must be used during analysis. If the result of the determination cannot be verified, the sample should be treated in one or more of the following ways:

6.2.2 *Serial Dilution*—Successively dilute and reanalyze the sample using spiking verifications to determine if the interference can be eliminated. This assumes that the analyte occurs at a sufficiently high concentration.

6.2.3 *Matrix Modification*—Matrix modifiers are frequently used to stabilize volatile or moderately volatile analyte metals such as lead, cadmium, chromium, and nickel. Metals such as these begin to volatilize at very low temperatures and require that the charring/ashing temperature be lowered. Lower charring/ashing temperatures reduce the chance of removing potential interferents from the matrix during the charring/ashing step. Adding certain chemical compounds or combinations of chemical compounds will reduce the volatility of selected metals by the formation of less volatile compounds during the charring/ashing process. The use of ammonium dihydrogen phosphate or phosphoric acid results in higher volatilization temperatures for many elements, thus permitting the use of higher charring/ashing temperatures to remove or reduce matrix interferences. Nickel nitrate has been shown to perform the same role for arsenic and selenium by forming high temperature arsenides and selenides. An alternate approach to the same problem is to reduce the temperature at which the matrix volatilizes, permitting it to be removed at a

lower charring/ashing temperature. Sodium chloride in seawater can be volatilized by adding ammonium nitrate as a matrix modifier. The sodium nitrate and ammonium chloride formed are more volatile than the sodium chloride and can be volatilized at much lower charring/ashing temperatures. Other matrix modifiers include various organic acids such as citric and ascorbic acid. These acids are believed to reduce matrix interferences by preventing the formation of large salt crystals that can occlude the analyte. A table of additional matrix modifiers is given in Appendix X1. See also the literature (2–18).

6.2.4 Platform Furnaces—The pseudo-constant temperature furnace design suggested by L’Vov (1) has minimized matrix and gas phase interference problems. L’Vov placed a graphite platform inside the graphite tube furnace to approximate a constant temperature design. Since the platform is heated by radiation, it lags behind the tube walls in temperature, and delays the atomization of the analyte until the tube atmosphere is at a higher, more constant temperature. This results in reduced vapor-phase condensation and reduces the effect of the sample matrix on the analyte signal. The integrated absorbance signal is proportional to the number of atoms in the sample, independent of the rate at which atomization occurs. This type of furnace is commercially available or the modification can be made by the user (19).

6.2.5 Standard Additions—Analyze the sample by method of standard additions while noting the precautions and limitations of its use. See 12.4.

6.3 Gases generated in the furnace during the atomization may have molecular absorption bands encompassing the analytical wavelength. When this occurs, either using background correction or choosing an alternative wavelength outside the absorption band should eliminate this interference. Nonspecific broadband absorption interference can also be compensated by background correction.

6.4 Memory effects occur if, during atomization, all the analyte is not volatilized and removed from the furnace. This condition is dependent on several factors, such as the volatility of the element and its chemical form, whether pyrolytic graphite is used, the rate of atomization, and furnace design. If this situation is detected through blank burns, the tube must be cleaned by operating the furnace at full power for the required time period at regular intervals in the analytical scheme.

6.5 Interference from a smoke-producing sample matrix can sometimes be reduced by extending the charring time at a higher temperature. Also, some instruments utilize an ashing cycle in the presence of air. Take care, however, to prevent loss of analyte.

6.6 Samples containing large amounts of organic material should be oxidized by conventional acid digestion prior to being placed in the furnace. In this way, broadband absorption will be minimized. The use of expendable-type laboratory ware should be considered to limit contamination.

6.7 Carbide formation, resulting from the chemical environment of the furnace, has been observed with certain elements that form carbides at high temperatures. Barium, molybdenum, nickel, titanium, and vanadium may be cited as examples. When this takes place, the element will be released very slowly

from the carbide and longer atomization times may be required before the signal returns to baseline levels. This problem is greatly reduced and sensitivity increases with the use of pyrolytically coated graphite.

6.8 Ionization interferences have to date not been reported with furnace techniques.

6.9 Contamination of the sample can be a major source of error because of the extreme sensitivities achieved with the furnace. Keep the sample preparation work area scrupulously clean (see 9.1). Clean all glassware with dilute $\text{HNO}_3(1 + 1)$. Pipette tips have been known to be a source of contamination. If suspected, acid soak them with $\text{HNO}_3(1 + 1)$ and rinse thoroughly with water. The use of only high-quality pipette tips greatly reduces this problem. It is very important that special attention be given to reagent blanks in both the analysis and the correction of analytical results. Lastly, pyrolytic graphite, because of the production process and handling, can become contaminated. As many as five, to possibly ten, high-temperature burns may be required to clean the tube before use.

6.10 Oxide formation is greatly reduced because atomization occurs in an inert atmosphere.

6.11 Several investigators who have studied interferences in the graphite furnace have concluded that nitrate is the preferred anion of the matrix. Therefore, nitric acid is preferable for any digestion or solubilization step. If the situation absolutely requires the use of another acid in addition to HNO_3 , or in place of HNO_3 (for example, tin), use the minimum amount of acid. This applies particularly to hydrochloric and perchloric acids, but also to sulfuric and phosphoric acids to a lesser extent.

7. Apparatus

7.1 Atomic Absorption Spectrophotometer—Single- or dual-channel, single- or double-beam instrument having a grating monochromator, photomultiplier detector, adjustable slits, wavelength range from 190 to 800 nm, and simultaneous background correction.

7.2 Hollow-Cathode Lamps—Single-element lamps are preferred but multi-element lamps may be used. Electrodeless discharge lamps may also be used when available, and are preferred for elements such as As, Se, Sb.

7.3 Graphite Tubes—Graphite tubes should be compatible with furnace device. Pyrolytically coated graphite tubes are recommended.

7.4 Data System—Data are collected using internal microprocessor or external desktop computer systems. Data can be stored on disks, transmitted to central servers, or printed in hard copy. Data may be evaluated and processed using the instrument’s dedicated systems to determine analyte concentrations. Users of this practice may use a strip chart recorder to obtain sample and calibration data, if desired.

7.5 Automatic sampling should be used. Studies have shown that the coefficient of variation for aqueous samples varies from 0.4 to 1.5 %, depending upon the metal and concentration (20).

8. Reagents and Materials

8.1 Purity of Reagents—It is intended that all reagents conform to the specifications of the Committee on Analytical

Reagents of the American Chemical Society as a minimum when such specifications are available.⁴ The high sensitivity of graphite furnace atomic absorption spectrophotometry may require reagents of a higher purity. Stock standard solutions are prepared from high-purity metals, oxides, or nonhygroscopic reagent grade salts using water and ultrapure nitric acid. Sulfuric, hydrochloric, and phosphoric acids are to be avoided wherever possible as they produce an adverse effect on many elements. A lesser grade of nitric acid and reagents may be used, provided it is first ascertained that the reagent is of sufficiently high purity to permit its use without lessening the accuracy of the determination.

8.2 Purity of Water— Unless otherwise indicated, references to water shall be understood to mean reagent water conforming to Type I of Specification D 1193. Other reagent water types may be used, provided it is first ascertained that the water is of sufficiently high purity to permit its use without lessening the bias and precision of the determination.

8.3 Nitric Acid (sp gr 1.42)—Distilled ultrapure concentrated nitric acid (HNO₃).⁵

8.4 Standard Solution, Stock (1 mL = 1 mg element)—Prepare each stock solution at a concentration of 1000 mg of the element per liter. Commercially available standard solutions may also be used.

8.5 Argon, standard, welders grade, commercially available. Nitrogen, argon with 5 % hydrogen, and hydrogen may also be used if recommended by the instrument manufacturer. The analyst should be aware that moisture present in some grades of inert gas may cause interference. The use of dry or moisture-free inert gas is suggested.

9. Samples and Sampling Procedures

9.1 Sample Handling— For the determination of trace elements, contamination and loss are of prime concern. Dust in the laboratory environment, impurities in reagents, and impurities on laboratory apparatus that the sample contacts are all sources of potential contamination. Sample containers can introduce either positive or negative errors in the measurement of trace elements by: (a) contributing contaminants through leaching or surface desorption, and (b) by depleting concentrations through absorption. Thus, the collection and treatment of the sample prior to analysis requires particular attention (see 6.8).

9.2 Sample Collection—Collect all samples in accordance with Specification D 1192 and Practices D 3370.

9.3 Sample Containers—Store the sample in a clean glass, linear polyethylene, polypropylene, or TFE-fluorocarbon container.

9.4 Sample Size— Sample size must be sufficient to allow for the determination. In general, use microliter sample ali-

quots for the analysis. However, when sample processing or multiple analyses, or both, are required, larger sample volumes may be necessary.

9.5 Sample Preservation—In most cases, samples are preserved by adding HNO₃ to a pH of less than 2. However, certain metals may require a different type of preservation. The analyst should refer to the specific method for guidance. If only dissolved elements are to be determined, filter the sample through a 0.45-μm membrane filter before adding acid. Filter and preserve as soon as possible, preferably at the time of collection.

9.6 Sample Storage— Analyze samples containing trace concentrations of analyte as soon as possible, preferable at the time of collection. The holding time for the samples may be calculated in accordance with Practice D 4841.

10. Preparation of Atomic Absorption Spectrophotometer

10.1 Furnace Device— Mount the furnace device in accordance with the instructions provided by the instrument manufacturer.

10.2 Turn on the instrument and allow the warm-up as instructed by the instrument manufacturer.

11. Calibration and Standardization

11.1 Initially set up the instrument in accordance with the manufacturer's specifications. Because of the differences between the various makes and models of satisfactory instruments, no detailed operating instructions can be given. Instead, the analyst should follow the instructions provided by the manufacturer for optimizing the drying temperature and time, the charring/ashing temperature and time, and the atomization temperature (or setting) and time.

11.1.1 With electrothermal (or furnace) atomization, background correction becomes of great importance especially at wavelengths less than 350 nm. This is because certain samples, when atomized, absorb or scatter light from the hollow-cathode lamp. This condition can be caused by the presence of gaseous molecular species, salt particles, or particulate matter in the sample beam. If no correction is made, sample absorbance will be greater than it should be, and the analytical result will be erroneously high. Background correction is discussed in 6.1.

11.1.2 Some analytical equipment provides for the interruption of the inert or sheath gas flow during the atomization step. This interruption has the advantage of reducing to a minimum the convection of the sample out of the optical beam, and therefore increasing sensitivity. At the same time, gas interruption also increases the unwanted matrix material in the optical beam, usually an undesirable condition. In general, the "gas-interrupt" option should not be used unless the absolute maximum analytical sensitivity is required and the increase in "background" or matrix signal is not harmful. Analyze both samples and standards using identical gas flow conditions. Systems not having "gas-interrupt" features will not necessarily have lower sensitivities.

11.2 Prepare calibration standards by diluting stock solutions at the time of analysis. For best results, prepare these calibration standard solutions daily, or as required, and discard after use. Prepare a blank and at least three calibration standards in graduated amounts in the appropriate range. Space

⁴ *Reagent Chemicals, American Chemical Society Specifications*, American Chemical Society, Washington, DC. For suggestions on the testing of reagents not listed by the American Chemical Society, see *Analar Standards for Laboratory Chemicals*, BDH Ltd., Poole, Dorset, U.K., and the *United States Pharmacopeia and National Formulary*, U.S. Pharmaceutical Convention, Inc. (USPC), Rockville, MD.

⁵ Commercially available Spectrograde or Utrex grade of acids have been found satisfactory for this purpose.

the calibration standards evenly in concentrations from 0 to 20 % greater than the highest expected value. Prepare the calibration standards with the same acid and at the same acid concentration as will result in the sample to be analyzed either directly or after processing.

11.3 Beginning with the blank and working toward the highest standard, analyze the solutions and record the readings.

11.4 Using the electronic data system on the instrument, construct an analytical curve by plotting the absorbances of standards versus their concentrations. Verify an acceptable correlation coefficient for the standard curve. Read results directly in concentration units.

11.4.1 Prepare a new analytical curve for each new series of samples.

12. Samples Analysis Procedure

12.1 Inject a measured aliquot of sample into the furnace device, dry, char/ash, and atomize. If the concentration found is greater than the highest standard, dilute the sample to the same acid concentration and reanalyze or extend the standard curve by analyzing additional calibration standards. The use of multiple injections improves accuracy and helps to detect furnace pipetting errors. It is strongly recommended that the same volume of sample be injected as was used for preparation of the analytical curve.

12.1.1 When the sample to be analyzed contains little or no suspended particles, prior digestion of the sample may not be required. The analyst is responsible for determining the need for sample digestion. The analyst should be aware that digestion would provide for a more uniform matrix and possibly lessen matrix effects for the sample containing dissolved organic material.

12.2 To verify the absence of interference, follow the procedure as given earlier in 6.1.1.

12.3 Analyze a check standard after approximately every ten sample injections to monitor the life and performance of the graphite tube. Lack of reproducibility or significant change in the signal for the standard indicates that the tube should be replaced. Tube life depends on sample matrix and atomization temperature, and a conservative estimate is that a tube will last at least 150 firings. A pyrolytic coating extends that estimate by a factor of about three.

12.4 If the method of standard additions is required (6.2.5), use four equal aliquots of sample. Dilute the first aliquot to a known volume with water. Add different known amounts of the test element to each of the second, third, and fourth aliquots before they are diluted to the same volume with water, so that the final solutions contain different additions of the analyte. Maintain the concentration of acid and matrix modifiers, if added, at approximately the same level for all four solutions. The volume of all four final solutions must be identical. Using the instrument's software, determine the absorbance of each solution and prepare a graph showing absorbance versus concentration. Scale the vertical axis in absorbance and the horizontal axis in concentrations of the known additions. Scale the abscissa to the left of the ordinate the same as to the right of the ordinate. Plot the absorbances of the four solutions on the graph and extrapolate the resulting line back to zero absorbance. The intercept with the abscissa on the left of the

ordinate is the concentration of the unknown. For the method of standard additions to be valid, take the following limitations into consideration:

12.4.1 The absorbance plot of sample and standards must be linear over the concentration range of concern. For best results, the slope of the plot should be nearly the same as the slope of the aqueous analytical curve. If the slope is significantly different, repeat the exercise using a greater sample dilution.

12.4.2 The effect of the interference should remain constant as the ratio of analyte concentration to sample matrix changes.

12.4.3 The standard addition should respond in a similar manner as the analyte.

12.4.4 The determination must be free of spectral interference and must be corrected for nonspecific background interference.

13. Calculation

13.1 Calculate the concentration of analyte in each sample, in micrograms per liter, using 11.4. It is strongly recommended that samples and standards be analyzed using identical volumes inasmuch as absolute weights of the elements are determined.

14. Precision and Bias

14.1 Precision and bias statements are included with each individual standard test method for which the technique is applicable and should conform to Practice D 2777.

15. Quality Control

15.1 In order to be certain that analytical values obtained using these test methods are valid and accurate within the confidence limits of the test, the following QC procedures must be followed when analyzing trace elements in water and wastewater by graphite furnace atomic absorption spectrophotometry.

15.2 *Calibration and Calibration Verification:*

15.2.1 Analyze at least three working standards containing concentrations of each element that bracket the expected sample concentration, prior to analysis of samples, to calibrate the instrument. The calibration correlation coefficient shall be equal to or greater than 0.990. In addition to the initial calibration blank, a calibration blank shall be analyzed at the end of the batch run to ensure contamination was not a problem during the batch analysis.

15.2.2 Verify instrument calibration after standardization by analyzing a standard at the concentration of one of the calibration standards. The concentration of a mid-range standard should fall within +/- 15% of the known concentration.

15.2.3 If calibration cannot be verified, recalibrate the instrument.

15.3 *Initial Demonstration of Laboratory Capability :*

15.3.1 If a laboratory has not performed the test before, or if there has been a major change in the measurement system, for example, new analyst, new instrument, and so forth, a precision and bias study must be performed to demonstrate laboratory capability.

15.3.2 Analyze seven replicates of a standard solution prepared from an Independent Reference Material containing a midrange concentration of each element. The matrix and

chemistry of the solution should be equivalent to the solution used in the collaborative study. Each replicate must be taken through the complete analytical test method including any sample preservation and pretreatment steps. The replicates may be interspersed with samples.

15.3.3 Calculate the mean and standard deviation of the seven values and compare to the acceptable ranges of bias. This study should be repeated until the recoveries are within acceptable limits. If a concentration other than the recommended concentration is used, refer to Practice D5847 for information on applying the F test and t test in evaluating the acceptability of the mean and standard deviation.

15.4 *Laboratory Control Sample (LCS):*

15.4.1 To ensure that the test method is in control, analyze a LCS containing a known concentration of each element with each batch or ten samples. If large numbers of samples are analyzed in the batch, analyze the LCS after every ten samples. The laboratory control samples for a large batch should cover the analytical range when possible. The LCS must be taken through all of the steps of the analytical method including sample preservation and pretreatment. The result obtained for a mid-range LCS shall fall within +/- 15 % of the known concentration.

15.4.2 If the result is not within these limits, analysis of samples is halted until the problem is corrected, and either all the samples in the batch must be reanalyzed, or the results must be qualified with an indication that they do not fall within the performance criteria of the test method.

15.5 *Method Blank:*

15.5.1 Analyze a reagent water test blank with each batch. The concentration of each element found in the blank should be less than 0.5 times the lowest calibration standard. If the concentration of each element is found above this level, analysis of samples is halted until the contamination is eliminated, and a blank shows no contamination at or above this level, or the results must be qualified with an indication that they do not fall within the performance criteria of the test method.

15.6 *Matrix Spike (MS):*

15.6.1 To check for interferences in the specific matrix being tested, perform a MS on at least one sample from each batch by spiking an aliquot of the sample with a known concentration of each element and taking it through the analytical method.

15.6.2 The spike concentration plus the background concentration of each element must not exceed the high calibration standard. The spike must produce a concentration in the spiked sample that is 2 to 5 times the analyte concentration in the

unspiked sample, or 10 to 50 times the detection limit of the test method, whichever is greater.

15.6.3 Calculate the percent recovery of the spike (P) using the following formula:

$$P = 100 \frac{[A(V_s + V) - BV_s]}{CV} \quad (1)$$

where:

- A = analyte concentration (mg/L) in spiked sample,
- B = analyte concentration (mg/L) in unspiked sample,
- C = concentration (mg/L) of analyte in spiking solution,
- V_s = volume (mL) of sample used, and
- V = volume (mL) added with spike.

15.6.4 The percent recovery of the spike shall fall within the limits, based on the analyte concentration, listed in Test Method D 5810, Table 1. If the percent recovery is not within these limits, a matrix interference may be present in the sample selected for spiking. Under these circumstances, one of the following remedies must be employed: the matrix interference must be removed, all samples in the batch must be analyzed by a test method not affected by the matrix interference, or the results must be qualified with an indication that they do not fall within the performance criteria of the test method.

NOTE 1—Acceptable spike recoveries are dependent on the concentration of the component of interest. See Test Method D 5810 for additional information.

15.7 *Duplicate:*

15.7.1 To check the precision of sample analyses, analyze a sample in duplicate with each batch. If the concentration of the analyte is less than five times the detection limit for the analyte, a matrix spike duplicate (MSD) should be used.

15.7.2 Calculate the standard deviation of the duplicate values and compare to the precision in the collaborative study using an F test. Refer to 6.4.4 of Practice D 5847 for information on applying the F test.

15.7.3 If the result exceeds the precision limit, the batch must be reanalyzed or the results must be qualified with an indication that they do not fall within the performance criteria of the test method.

15.8 *Independent Reference Material (IRM):*

15.8.1 In order to verify the quantitative value produced by the test method, analyze an Independent Reference Material (IRM) submitted as a regular sample (if practical) to the laboratory at least once per quarter. The concentration of the IRM should be in the concentration mid-range for the method chosen. The value obtained must fall within the control limits established by the laboratory.

16. Keywords

16.1 elements; graphite furnace atomic absorption; water

APPENDIX

(Nonmandatory Information)

X1. MATRIX MODIFIERS

X1.1 The Table X1.1 presents a list of matrix modifiers and their usage. References to the literature are also included. It is the responsibility of the analyst to determine the applicability of a matrix modifier to a specific sample matrix.

TABLE X1.1 Selected List of Matrix Modifiers

Element	Modifier	Matrix	Reference
As	nickel nitrate	all types	2, 3
	ammonium nitrate	seawater	2
Cd	EDTA	seawater	4
	citric acid	seawater	5
Cu	Na ₂ O ₂	seawater	6
	ascorbic acid	seawater	7, 8
Ni	ammonium dihydrogen phosphate	blood, liver, urine	9
	lanthanum nitrate	seawater	10, 11
Pb	ammonium nitrate	seawater	12, 13
	nickel nitrate	all types	2, 14
Se	Cu, Fe, Mn, and Zn nitrates	all types	15, 16
	ammonium nitrate	seawater	17
Zn	citric acid	seawater	18
	palladium nitrate	all types	21
Cd, Pb, As, Se			

REFERENCES

- (1) L'Vov, B. V., "The Way Towards Absolute Method of Atomic Absorption Analysis," *Spectrochimica Acta*, 33B, 153, 1977.
- (2) Ediger, R. D., "Atomic Absorption Analysis with Graphite Furnace Using Matrix Modification," *Atomic Absorption Newsletter*, Vol 14 (5), 1975, p. 127.
- (3) Chakraborti, D., DeJonghe, W., and Adams, F., "The Determination of Arsenic by Electrothermal Atomic Absorption Spectrometry with a Graphite Furnace," *Anal. Chim. Acta*, Vol 119, 1980, p. 331.
- (4) Guevremont, R., Sturgeon, R. E., and Berman, S. S., "Application of EDTA to Direct Graphite Furnace Atomic Absorption Analysis for Cadmium in Sea Water," *Anal. Chim. Acta*, Vol 115 (163), 1980, p. 163.
- (5) Guevremont, R., "Organic Matrix Modifiers for Direct Graphite Furnace Atomic Absorption Determination of Cadmium in Seawater," *Analytical Chemistry*, Vol 52 (11), 1980, p. 1574.
- (6) Churella, D. J., and Copeland, T. R., "Interference of Salt Matrices in the Determination of Copper by Atomic Absorption Spectrometry in Electrothermal Atomization," *Analytical Chemistry*, Vol 50 (2), 1978, p. 309.
- (7) Hydes, D. J., "Reduction of Matrix Effects with A Soluble Organic Acid in the Carbon Furnace Atomic Absorption Spectrometric Determination of Cobalt, Copper and Manganese in Sea Water," *Analytical Chemistry*, Vol 52, 1980, p. 959.
- (8) Regan, J. G. T., and Warren, J., "A Novel Approach to the Elimination of Matrix Interferences in Flameless Atomic Absorption Spectroscopy Using A Graphite Furnace," *Analyst*, Vol 101, 1976, p. 220.
- (9) Hinderberger, E. J., Kaiser, J. L. and Koirttyohann, S. R., "Furnace Atomic Absorption Analysis of Biological Samples Using the L'Vov Platform and Matrix Modification," *Atomic Spectroscopy*, Vol 2 (1), 1, (Jan.-Feb. 1981).
- (10) Thompson, K. C., Wagstaff, K., and Wheatstone, K. C., "Method for the Minimization of Matrix Interferences in the Determination of Lead and Cadmium in Nonsaline Waters by Atomic-Absorption Spectrophotometry Using Electrothermal Atomization," *Analyst*, Vol 102 (1213), 1977, p. 310.
- (11) Bengtsson, M., Danielsson, L. G., and Magnusson, B., "Determination of Cadmium and Lead in Sea Water After Extraction Using Electrothermal Atomization. Minimization of Interferences from Coextracted Sea Salts," *Analytical Letters*, Vol 12 (A13), 1979, p. 1367.
- (12) Frech, W., and Cedergren, A., "Investigations of Reactions Involved in Flameless Atomic Absorption Procedures Part III, A Study of Factors Influencing the Determination of Lead in Strong Sodium Chloride Solutions," *Anal. Chim. Acta*, Vol 88, 1977, p. 57.
- (13) Stein, V. B., Canelli, E., and Richards, A. H., "Simplified Determination of Cadmium, Lead and Chromium in Estuarine Waters by Flameless Atomic Absorption," *International Journal of Environmental Analytical Chemistry*, Vol 8, 1980, p. 99.
- (14) Martin, T. D., Kopp, J. R., and Ediger, R. D., "Determining Selenium in Water Using Graphite Furnace," *Atomic Absorption Newsletter*, Vol 14, 1975, p. 109.
- (15) Alexander, J., Saeed, K., and Thomassen, Y., "Thermal Stabilization of Inorganic and Organoselenium Compounds for Direct Electrothermal Atomic Absorption Spectrometry," *Anal. Chim. Acta*, Vol 120, 1980, p. 377.
- (16) Kamada, T., and Yamamoto, Y., "Use of Transition Elements to Enhance Sensitivity for Selenium Determination by GFAAS Combined with Solvent Extraction with the APDC-MIBK System," *Talanta*, Vol 32, 1980, p. 473.
- (17) Campbell, W. C., and Ottaway, J. M., "Direct Determination of Cadmium and Zinc in Sea Water by Carbon Furnace Atomic Absorption Spectrometry," *Analyst*, Vol 102 (1216), 1977, p. 495.
- (18) Guevremont, R., "Organic Matrix Modifiers for Direct Determination of Zinc in Seawater by Graphite Furnace Atomic Absorption Spectrometry," *Analytical Chemistry*, Vol 53, 1981, p. 911.
- (19) Hinderberger, E. J., Kaiser, J. L., and Koirttyohann, S. R., "Furnace Atomic Absorption Analysis of Biological Samples Using the L'Vov Platform and Matrix Modification," *Atomic Spectroscopy*, Vol 2 (1), 1, (Jan.-Feb. 1981).
- (20) Cooksey, M., and Barnett, W. B., "Matrix Modification and the Method of Addition in Flameless Atomic Absorption," *Atomic Absorption Newsletter*, Vol 18, 1979, p. 101.
- (21) Welz, Bernard, Schlemmer, Gerhard, and Mudakovic, JR, "Palladium Nitrate-Magnesium Nitrate Modifier for Graphite Furnace Atomic Absorption Spectrometry," *Journal of Analytical Atomic Spectrometry*, Jan. 1988, Vol 3, p. 93.

SUMMARY OF CHANGES

Committee D19 has identified the location of selected changes to this standard since the last issue (D 3919-99) that may impact the use of this standard.

- | | |
|---|--|
| <p>(1) Section 2 has D 2777, D 5819, and D 5847 added.</p> <p>(2) Spelling and grammar were corrected in sections 1.1, 6.1.1, 6.2.3, 6.3, 6.6, 6.9, and 12.1.1.</p> | <p>(3) Section 14.1 added conforming to D 2777.</p> <p>(4) The QC section 15 was added to the test method.</p> |
|---|--|

ASTM International takes no position respecting the validity of any patent rights asserted in connection with any item mentioned in this standard. Users of this standard are expressly advised that determination of the validity of any such patent rights, and the risk of infringement of such rights, are entirely their own responsibility.

This standard is subject to revision at any time by the responsible technical committee and must be reviewed every five years and if not revised, either reapproved or withdrawn. Your comments are invited either for revision of this standard or for additional standards and should be addressed to ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee, which you may attend. If you feel that your comments have not received a fair hearing you should make your views known to the ASTM Committee on Standards, at the address shown below.

This standard is copyrighted by ASTM International, 100 Barr Harbor Drive, PO Box C700, West Conshohocken, PA 19428-2959, United States. Individual reprints (single or multiple copies) of this standard may be obtained by contacting ASTM at the above address or at 610-832-9585 (phone), 610-832-9555 (fax), or service@astm.org (e-mail); or through the ASTM website (www.astm.org).